Baldwins Corners
Northerly
Montville Twp.

DIETZGEN
TRADE MARK

ENGINEERS'
LEVEL BOOK
No. 410

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

Baldwins Corners
North
Montville Twp
~~Clay St~~

Extension of Baldwins Cor. North
Road in Thompson Twp.
Back of book

INDEX See next pg.

BOOK 15

CLAY ST. SEC. G-H-I (pt.) C.H. 37

Align't, Sections & topo 2-27

Check levels, culverts & slopes 28-71

" 74-end

CLAY ST. SEC. I (north part) 72-73

BM No 10 Nail NW Root
Maple South Side Road
about 600 ft West Corners
Elev. 1271.00
Elev Pvt at Cross Roads
around 1264.15

BM No 9 South Root
24" Hickory South Side
Road 780 ft East Cross Roads
Elev 1270.50

Elev. Pvt inside edge
ong Road
1264.15

H.I.
1269.80

B.M. N.W. Cor. N. Head

445 1265.55

Conc.	100	50	1264.13	50	10.	
Sta 0+00	5.43	5.50	5.65	5.56	5.62	

1264.80

	25	14	13	12	4	11	13	14	25
1+00	5.4	5.3	5.8	5.1	5.0	5.2	6.0	5.7	6.0

1266.1

22-	25	14	13	11	4	12	13	14	25
2+00	3.4	4.2	4.6	4.0	3.7	3.7	4.3	3.8	4.8

1267.5

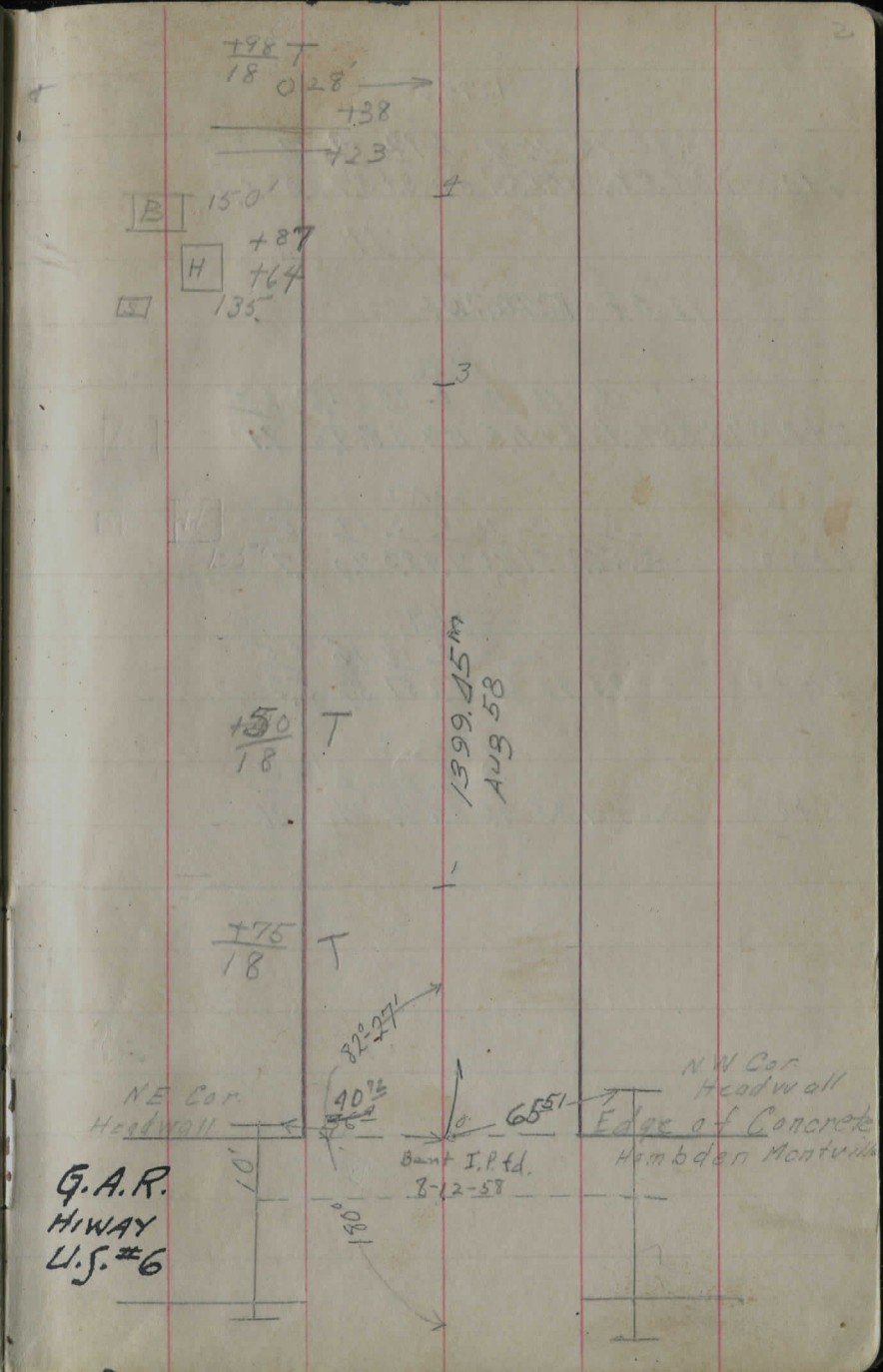
	25	14	13	12	4	14	15	16	25
3+00	1.4	2.9	3.3	2.7	2.3	2.3	2.9	2.5	3.3

143

25	13	10.5	8	1278.95		1269.05			
7.9	8.0	13	12	13	8	7	8	16	17	18	25
4+00		9.7	10.4	9.5	9.3	9.9	9.9	10.0	10.5	9.8	9.7

1271.95

	25	13	10	9	8	16	17	25
5+00	4.2	5.7	7.2	6.6	7.0	7.3	6.6	8.5



1275.65

	25	18	15	11	9	4	12	14	17	25
6+00	0.0	0.5	2.5	4.4	3.4	3.3	3.4	3.7	2.5	2.4

0.79

12.04 1290.20

1278.9

	25	18	14	11	10	4	14	18	25
7+00	07.7	8.5	10.4	12.4	11.5	11.3	11.5	9.2	9.4

1282.3

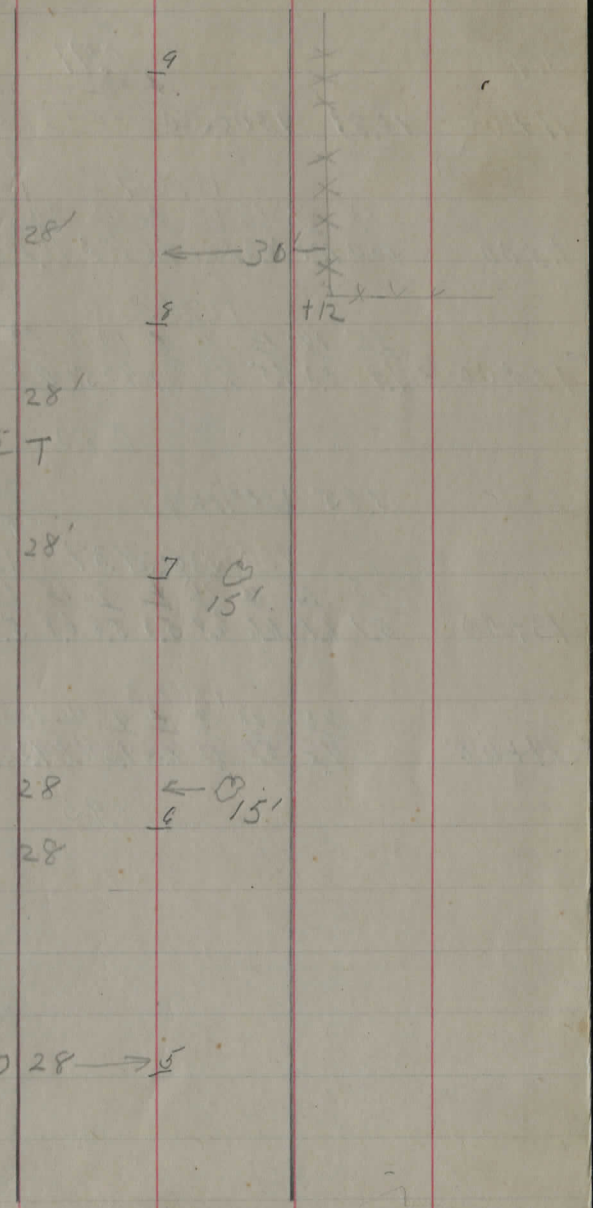
	25	17	12	10	4	13	19	25
8+00	5.6	6.0	8.9	8.2	7.9	8.3	7.0	6.7

1284.9

	25	14	12	14	13	16	25
9+00	4.3	4.9	6.9	5.3	5.7	5.2	5.2

1287.3

	25	18	12	10	4	10	12	25
10+00	3.2	3.4	3.6	3.2	2.9	2.8	3.4	3.4



0.71

10.81 1300.30

1290.7

	25	14	12	10	8	10	20	25
11+00	10.0	10.1	10.6	10.1	9.6	10.3	10.2	9.6

1296.4

	25	14	12	10	8	10	11	15	25
12+00	1.9	3.2	4.5	4.2	3.9	4.3	5.1	2.6	1.1

0.80

7.95 1302.45

BM No 1
BM. Spike in

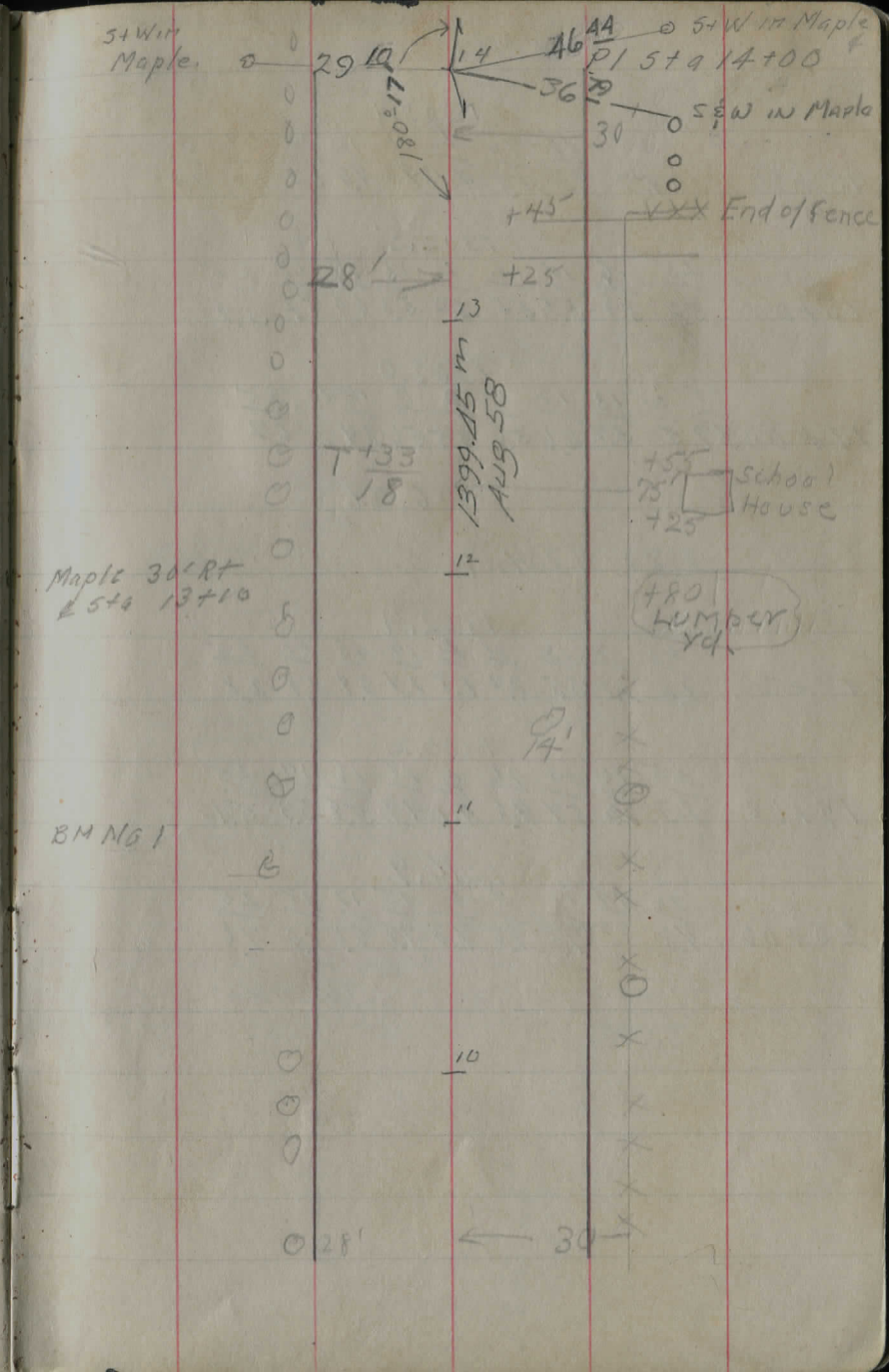
1302.37 1303.08

	25	15	13	10	8	9	12	13	25
13+00	5.7	6.1	6.4	6.0	6.3	5.8	6.4	5.9	5.0

1303.3

	25	13	8	8	9	11	12	20	25
14+00	4.8	5.0	4.3	4.2	4.3	4.9	4.3	3.6	

3.95



1307.45

1303.1

15+00	25 / 4.9	19 / 4.3	16 / 4.9	4 / 4.4	11 / 4.3	12 / 4.9	19 / 3.3	21 / 1.8	25 / 1.3

1302.5

16+00	25 / 5.2	16 / 5.1	14 / 5.8	12 / 5.5	4 / 5.0	13 / 5.3	14 / 6.0	17 / 5.2	25 / 3.9

1302.0

17+00	25 / 3.7	22 / 5.0	13 / 5.7	12 / 6.4	11 / 5.4	4 / 5.5	11 / 5.6	15-16 / 6.4	25 / 6.2

6.06.

2.80 1304.19

1302.4

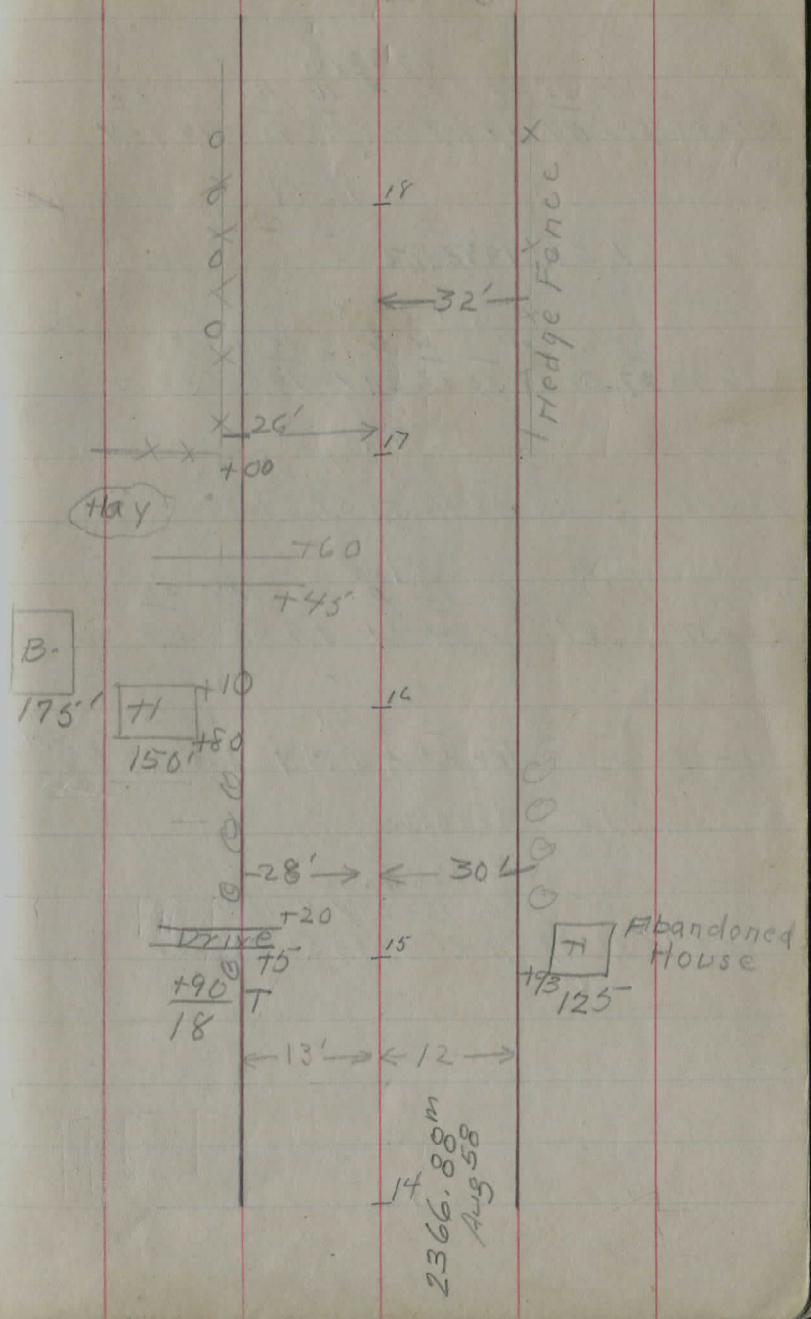
18+00	25 / 4.2	14 / 1.8	13 / 3.5	11 / 2.4	4 / 1.8	14 / 2.4	15 / 3.4	18 / 2.9	25 / 2.8

1300.2

19+00	25 / 2.7	16 / 3.3	13 / 5.4	11 / 4.6	4 / 4.0	14 / 4.9	16 / 5.8	17 / 5.3	25 / 5.1

1296.9

20+00	25 / 4.8	14 / 6.2	10 / 7.8	8 / 7.3	4 / 7.3	15 / 7.9	17 / 8.4	18 / 8.0	25 / 7.4



1292.6

21+00 25/7.5 18/8.3 12/11.1 16/12.8 8/11.8 ℄/11.6 14/11.8 16/12.5 17/11.4 25/10.7

11.48

1.01 1293.72

1289.8

22+00 25/2.7 15/3.2 11/4.3 13 10/5.0 9/4.3 ℄/3.9 13/4.2 14/4.8 15/4.3 25/3.8

1287.9

23+00 25/6.9 12/6.6 9/5.8 ℄/5.8 10/5.9 11/6.4 25/6.8

1287.6

23+31 300'/11.7 200/10.8 100'/9.8 65'/9.3 FL/9.1 12 12/6.4 ℄/6.1 9/5.9 9/5.8 FL/8.8

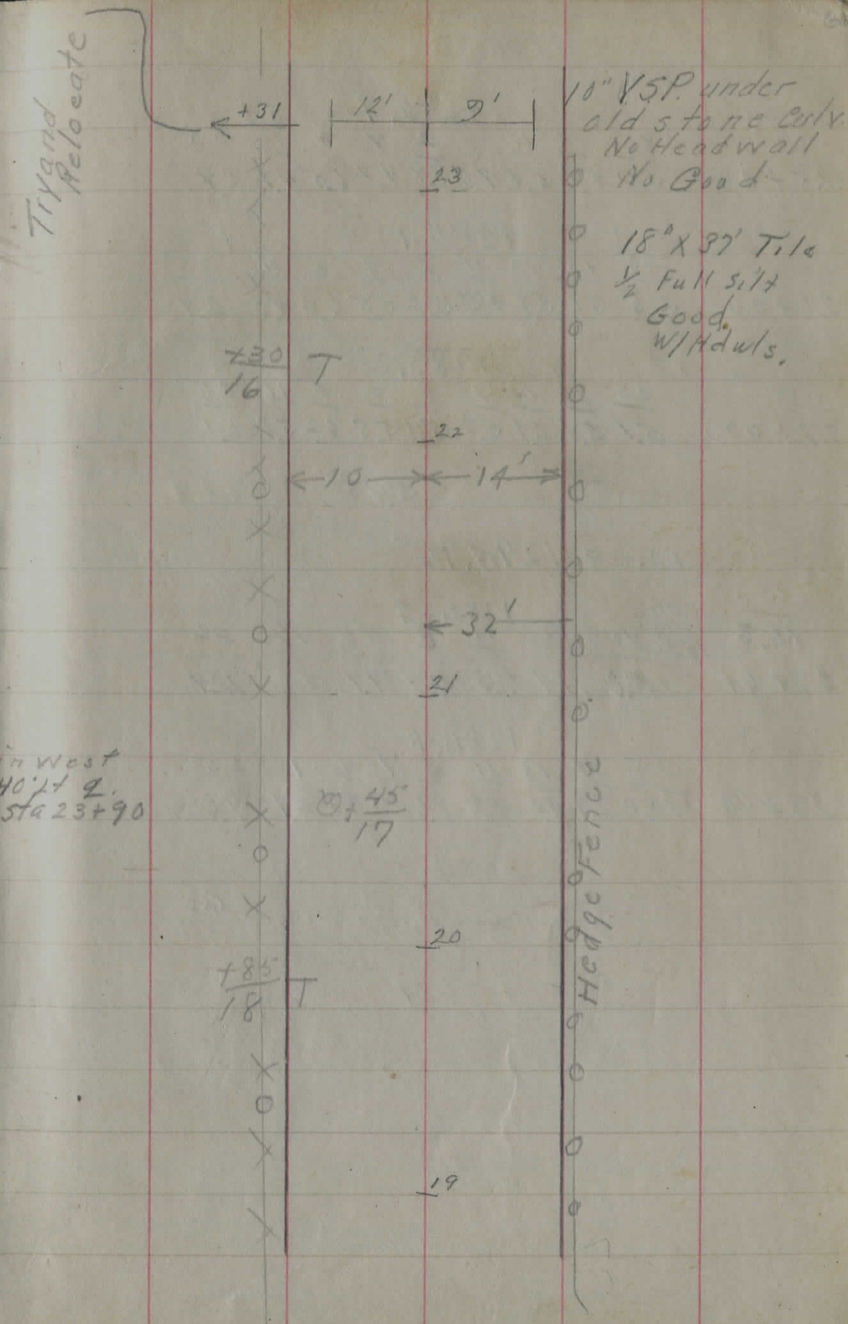
6.18 BM No 2 Spike in West Post Maple 40' Lt ℄ Sta 23+90

6.57 1287.15

3.18 1290.33

1286.2

24+00 25/3.1 13/3.8 12/4.9 10/4.1 ℄/4.1 7/4.3 8/5.1 10-12/3.7 25/3.5



1290.33

1285.9

	25	12	11	8	6	7	8	10	25
25+00	50	4.8	5.5	4.6	4.9	4.7	6.5	4.7	2.8

1285.1

	25	13	12	11	6	7	9	11	25
26+00	5.3	5.4	5.9	5.5	5.2	5.5	6.0	4.6	2.4

1285.2

	25	13	12	10	8	7	9	11	25
27+00	5.1	5.4	6.1	5.2	5.1	5.5	6.2	5.8	6.1

5.45

10.08 1294.96

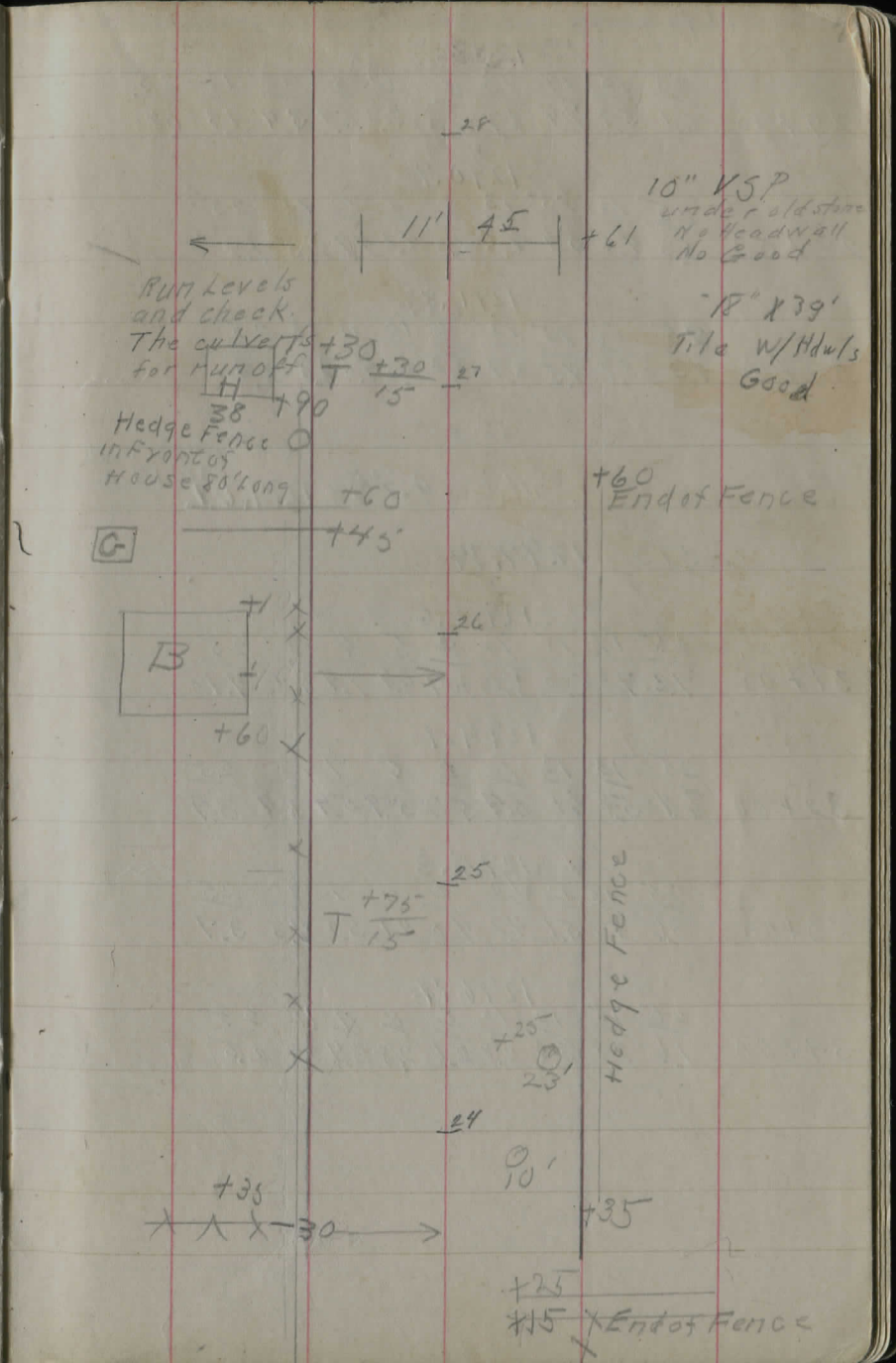
1285.9

30	200								
16.3	14.5	100	FL	11	6	4½	4½	FL	
27+61		13.3	11.4	9.5	9.1	9.4		11.4	

1286.4

	25	14	13	11	8	7	9	10	25
28+00	10.0	8.8	9.2	8.8	8.6	8.7	9.8	8.1	9.6

68



HI 1294.96

1288.8

	25	15	14	13	8	7	8	12	18	25
29+00	6.1	5.9	7.4	6.7	6.2	6.2	6.9	3.4	1.3	0.8

1290.7

	25	16	15	13	8	9	10	15	25
29+50	5.3	4.6	5.4	4.6	4.3	4.2	4.9	2.5	1.9

1291.8

	25	16	15	13	8	10	11	12	25
30+00	4.3	3.9	4.5	3.7	3.2	3.2	4.0	3.3	2.3

BM. #3 Spike in west 30' Rt @

0.75 1294.21

513 1299.34

1292.6

	25	17	15	12	8	5	6	8	25
31+00	7.3	7.3	8.0	7.0	6.7	6.9	7.4	6.2	4.1

1294.1

	25	13	12	10	8	6	7	8	25
32+00	6.4	5.8	6.1	5.4	5.2	5.4	5.9	5.4	3.9

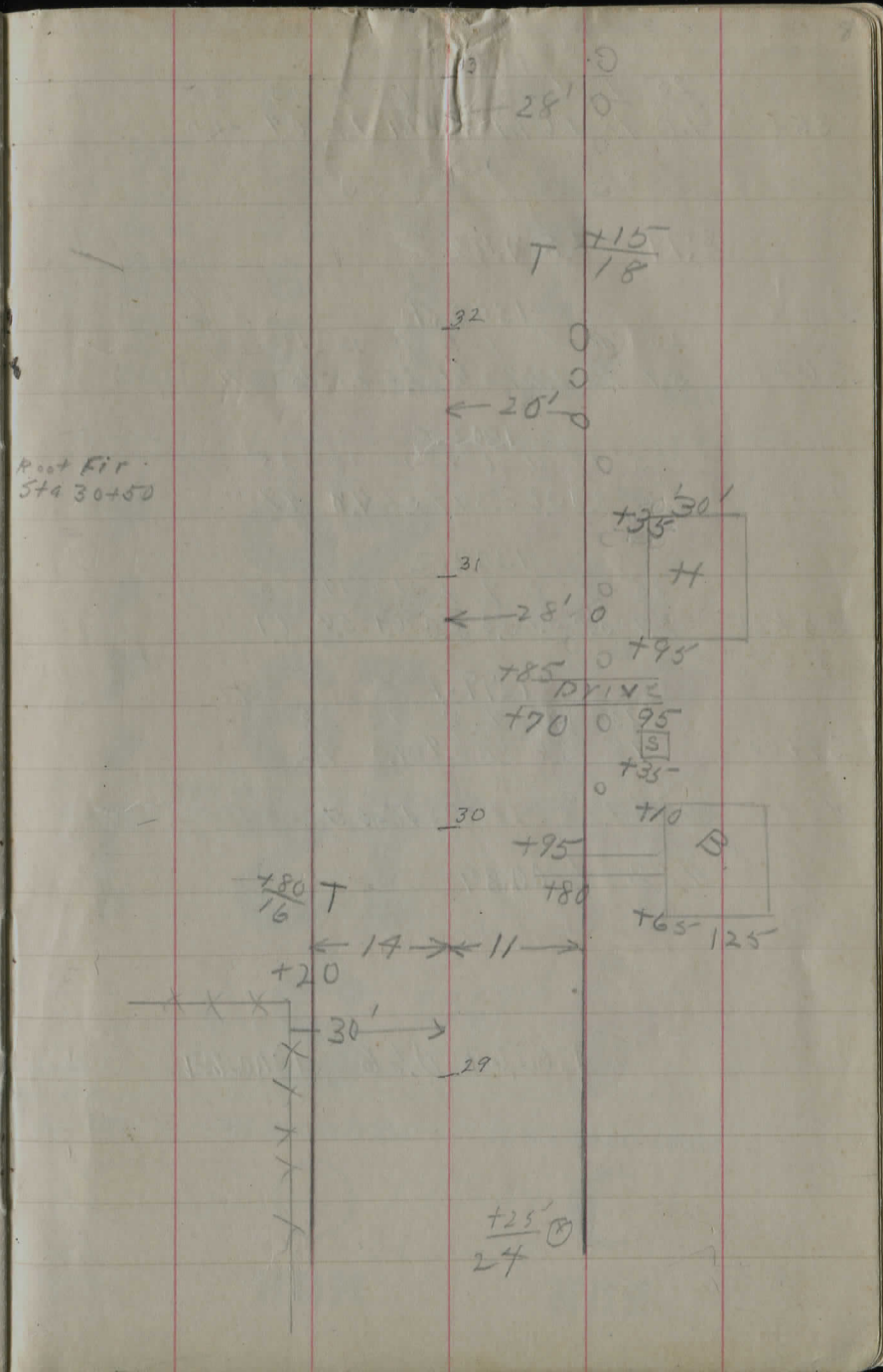
1295.3

	25	13	12	10	8	7	9	10	25
33+00	3.6	4.7	5.1	4.2	4.0	4.1	5.0	4.3	3.7

1296.7

	25	15	12	10	8	8	9	11	25
34+00	1.4	2.8	3.6	2.8	2.4	2.8	3.4	3.2	2.5

Root Fir
Sta 30+50



	25	13	12	[illegible]	[illegible]	10	12	13	25
35+00	-1.0	1.2	1.6	1.1	[illegible]	1.1	1.3	0.4	-1.0

0.53

8.71 1307.52

1300.4

	25	11	10	7	4	10	12	13	25
36+00	5.9	7.3	7.7	7.2	7.1	7.2	8.1	7.5	7.1

1302.8

	25	15	11	6	4	14	18	25
37+00	1.4	3.3	3.6	5.3	4.7	5.2	4.8	4.7

1302.2

	25	9	8	7	4	12	14	25
38+00	2.9	5.0	5.7	5.3	5.3	6.1	5.4	6.1

1299.1

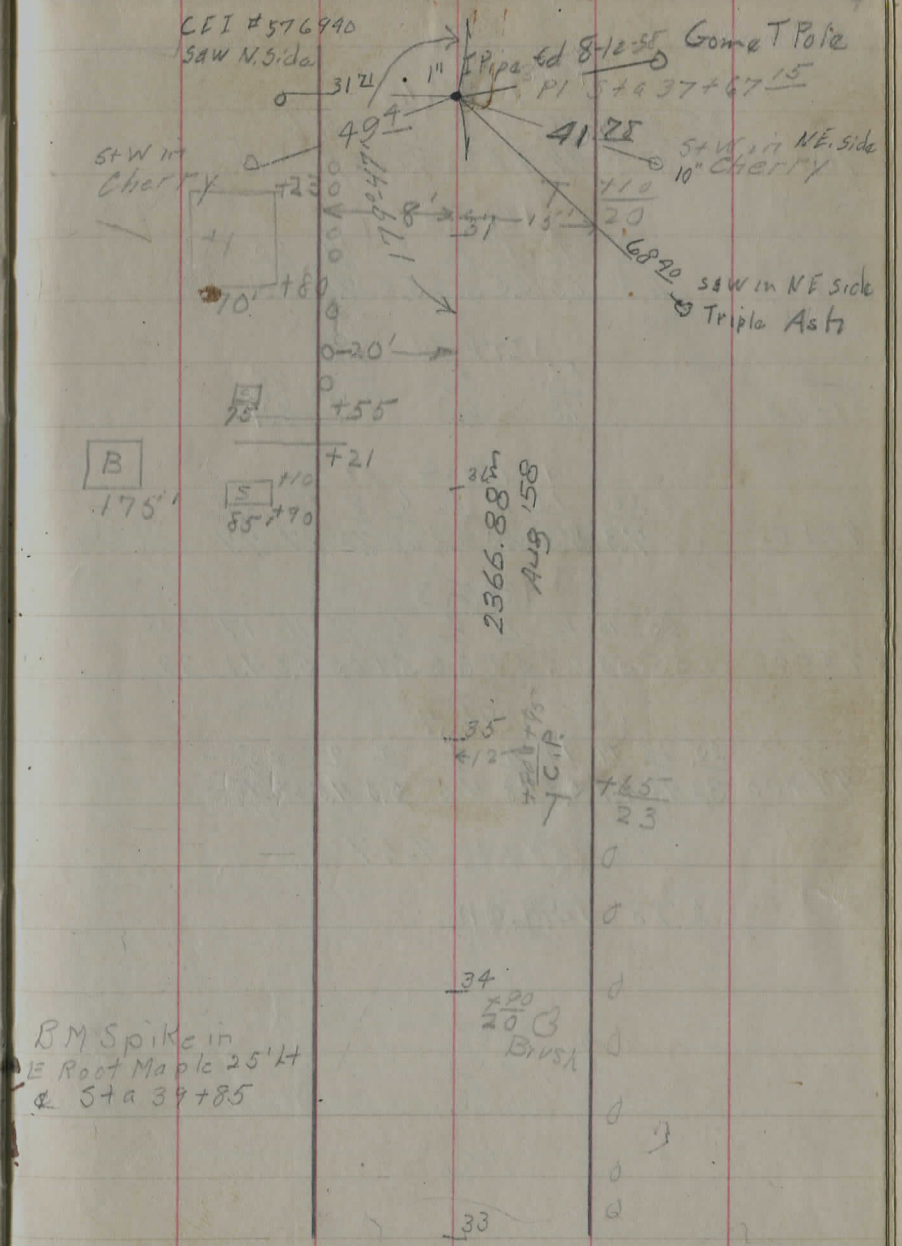
	25	15	9	4	12	25
39+00	4.8	5.4	8.9	8.4	9.0	9.2

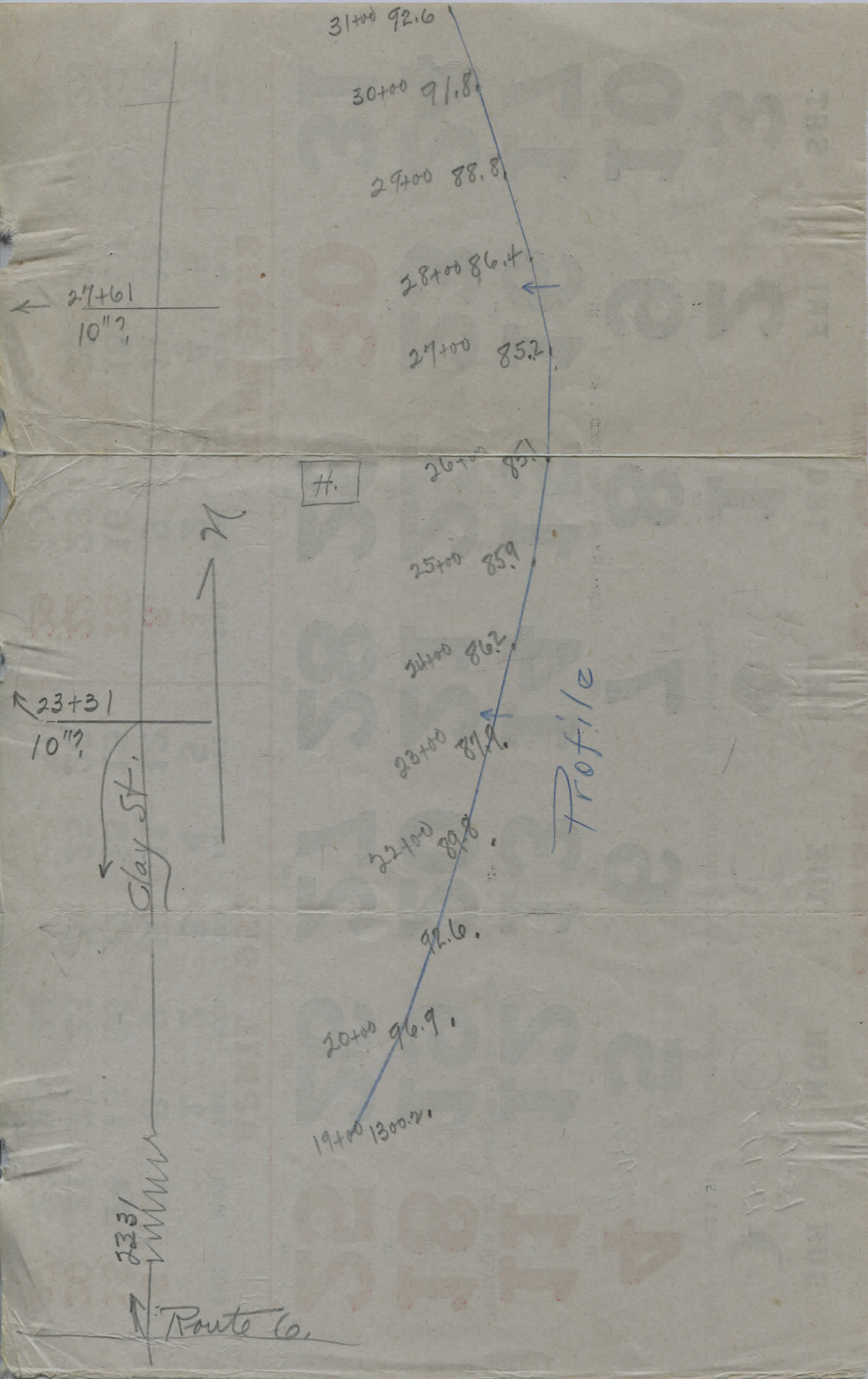
10.65

4.02 1300.89

BM #4

0.66 1300.23




31+00 92.6
30+00 91.8
29+00 88.8
28+00 86.4
27+00 85.2
26+00 85.1
25+00 85.9
24+00 86.2
23+00 87.9
22+00 89.8
92.6
20+00 96.9
19+00 1300.2
Profile
27+61
10"?
23+31
10"?
Clay St.
N
#.
2330'
Route 6.

1300.89

1297.1

40+00	25 / 0.9	17 / 3.7	11 / 3.4	10 / 4.4	9 / 4.1	8 / 3.8	8 / 4.1	25 / 6.0

1295.3

41+00	25 / 6.3	17 / 6.5	10 / 5.5	8 / 5.6	6 / 5.8	14 / 7.0	25 / 6.3

1294.9

41+73	FL / 7.8	8 / 6.0	FL / 7.7	25 / 8.9

1294.12

42+00	25 / 7.3	13 / 7.3	11 / 4.0	8 / 4.7	6 / 6.8	8 / 7.2	17 / 7.7	25 / 7.9

1295.3

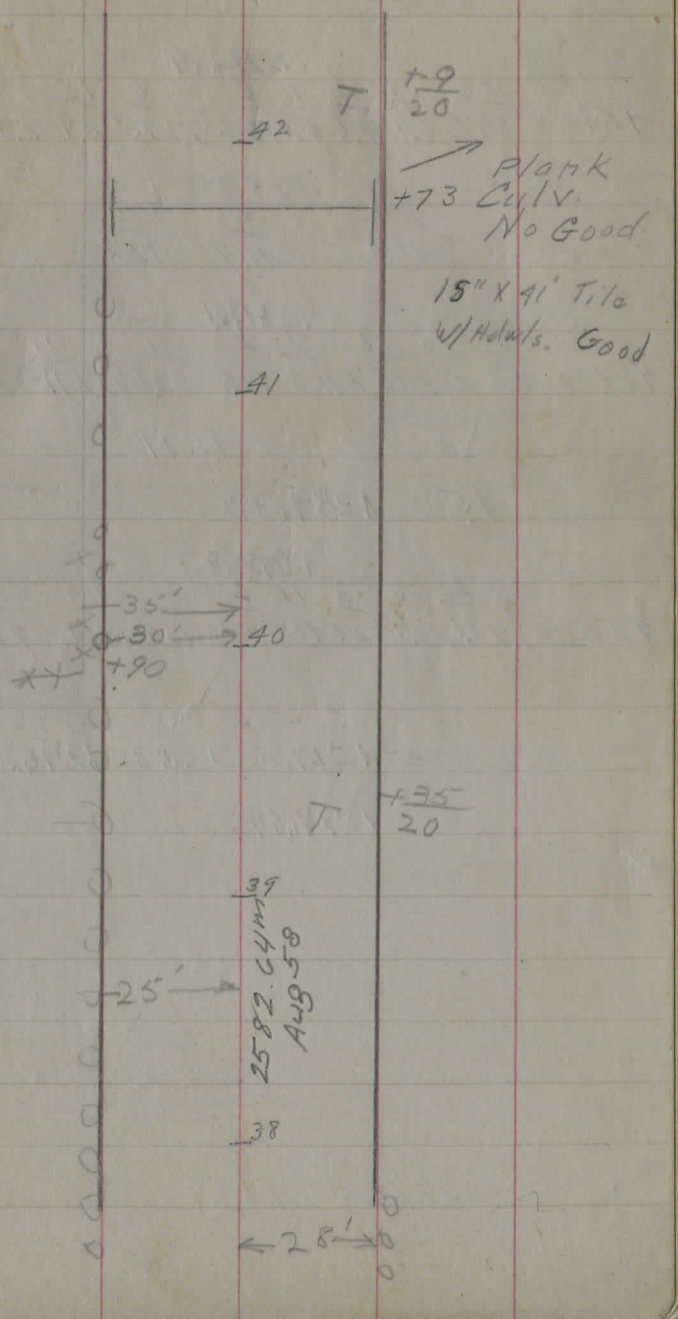
43+00	25 / 5.5	15 / 5.8	12 / 6.4	11 / 5.9	8 / 6.6	6 / 5.9	8 / 6.5	11 / 5.3	17 / 4.1	25 / 3.8

1296.14

44+00	25 / 3.2	18 / 4.0	14 / 4.7	13 / 5.3	11 / 4.8	8 / 4.5	8 / 5.3	9 / 4.5	25 / 4.7

4.67

2.78 1299.00



1299.00

30 / 0.7

1292.4

25	14	13	11	9	4	6	15	25
0.7	6.9	7.4	6.9	6.6	6.7	7.5	8.9	3.3

45+00

1287.6

FL		FL
13.4	11.4	12.7

1287.81

25	15	13	7	2	4	6	11	15	25
7.2	12.2	13.7	11.8	11.9	12.1	12.9	11.3	10.4	8.8

46+00

11.11

1.50 1289.39

1278.8

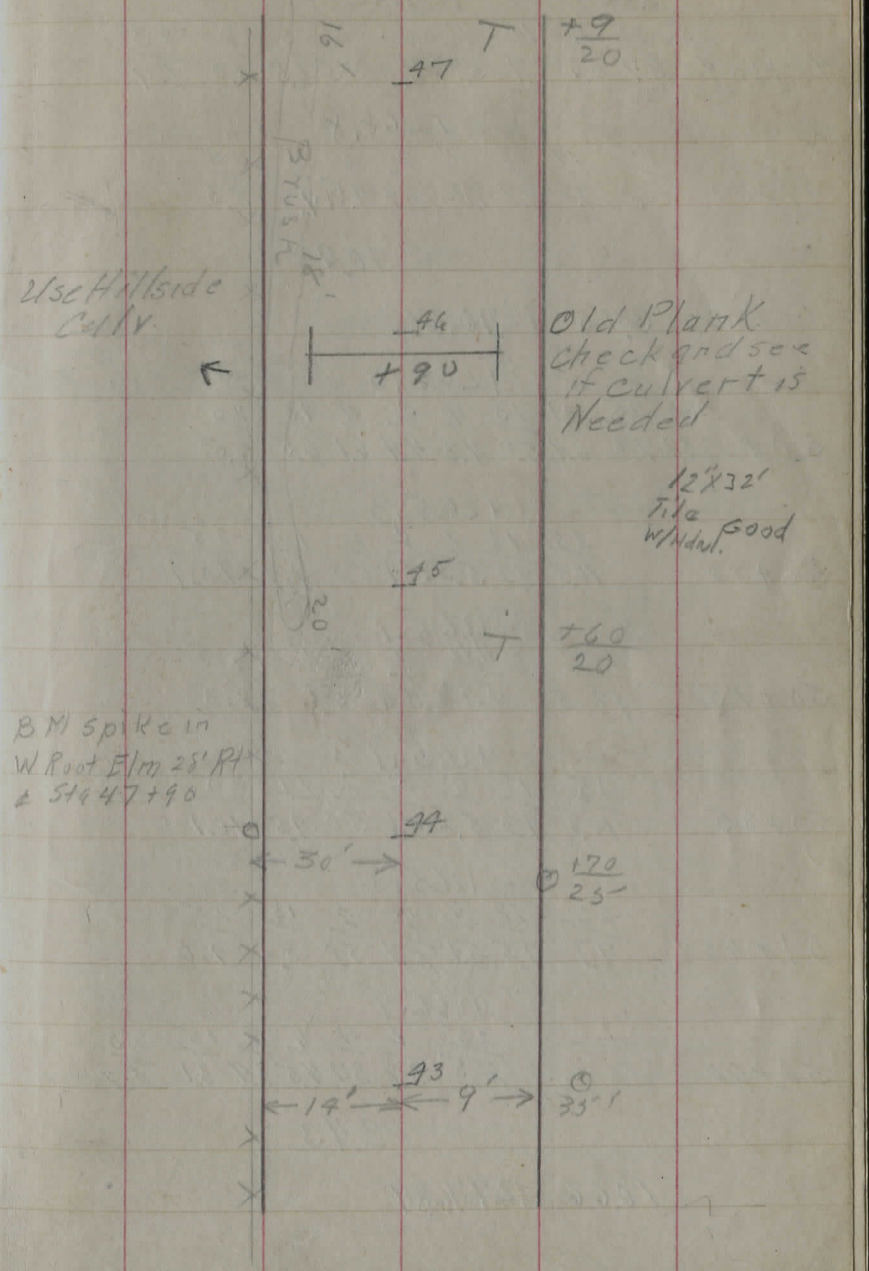
25	22	15	13	10	2	5	6	9	25
7.7	8.1	10.4	12.5	11.3	10.6	10.9	11.6	9.7	9.1

47+00

BM #5

12.58 1276.81

0.88 1277.69



1277.69 1272.2

48+00 — 25/1.0 22/3.7 16/5.6 14/6.7 11/5.8 9/5.5 3/5.5 5/6.5 8/5.0 25/1.9

1268.8

49+00 — 25/10.2 14/9.2 12/9.7 11/9.0 9/8.9 3/9.5 5/9.2 25/8.3

10.98

3.95 1270.66

1266.3

50+00 — 30/8.7 25/7.3 21/6.4 13/5.0 9/4.3 9/4.4 4/6.1 13/6.5 25/6.5

1265.3

50+70 — 25/10.5 16/9.2 9/5.3 9/5.4 4/5.0 10/9.9 25/10.1

1265.1

50+75 — FL/13.5 HW/5.9 9/5.6 HW/5.6 FL/12.3

1265.1

50+85 — 25/10.3 18/9.3 9/5.2 9/5.6 4/5.0 14/9.5 25/10.1

1265.3

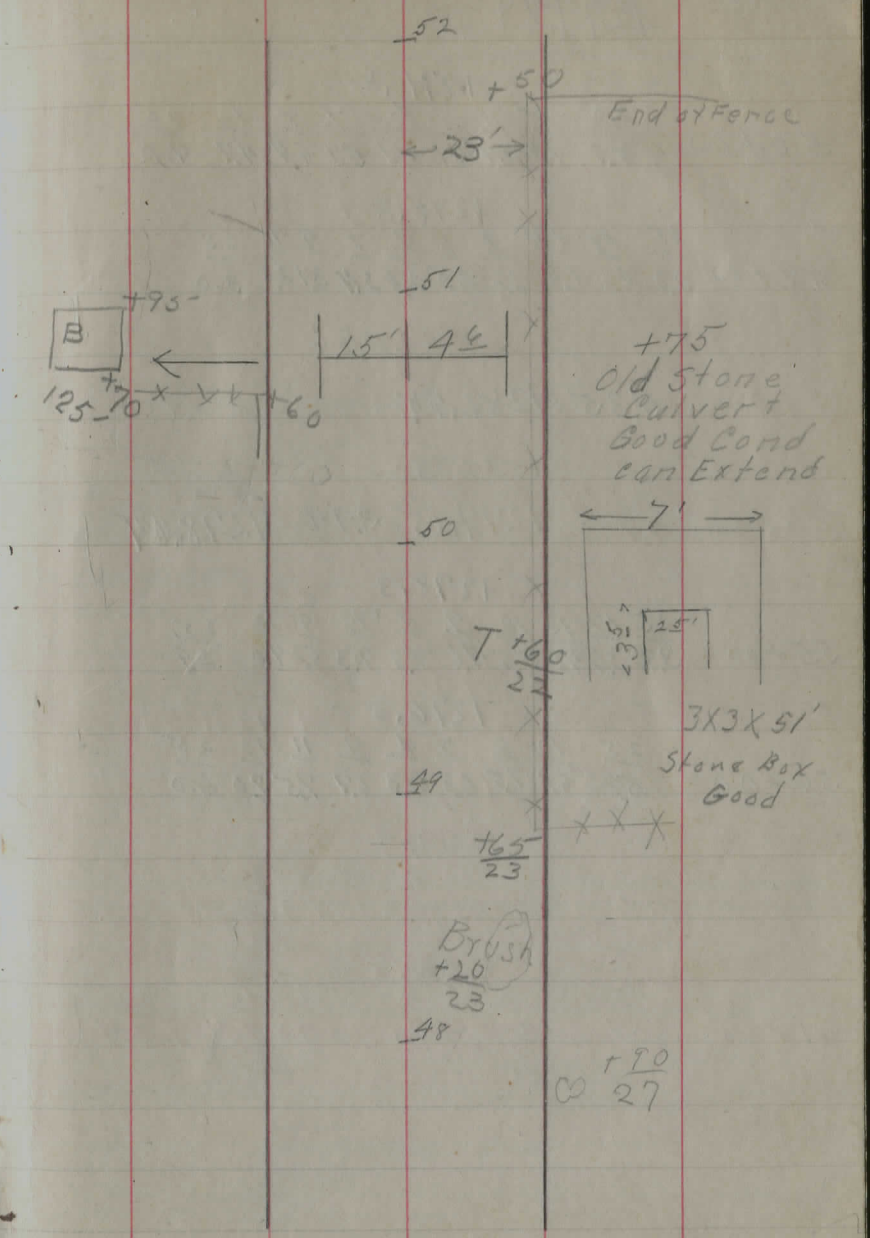
51+01 — 25/9.7 18/9.5 9/5.1 9/5.4 2/5.0 15/8.7 25/9.0

1266.9

52+00 — 25/2.5 4/3.8 4/3.7 4/4.5 8/3.4 15/3.1 25/0.8

3.43

10.66 1277.89



1277.89

1271.8

53+00	25 / 4.4	15 / 4.4	11 / 6.4	8 / 6.1	6 / 6.1	7 / 5.9	8 / 6.4	12 / 4.7	25 / 4.0

1275.8

54+00	25 / 0.3	19 / 0.6	13 / 1.6	9 / 3.2	8 / 2.5	6 / 2.1	7 / 2.4	9 / 3.1	11 / 2.8	25 / 3.0

0.66

5.35 1282.58

BM #6

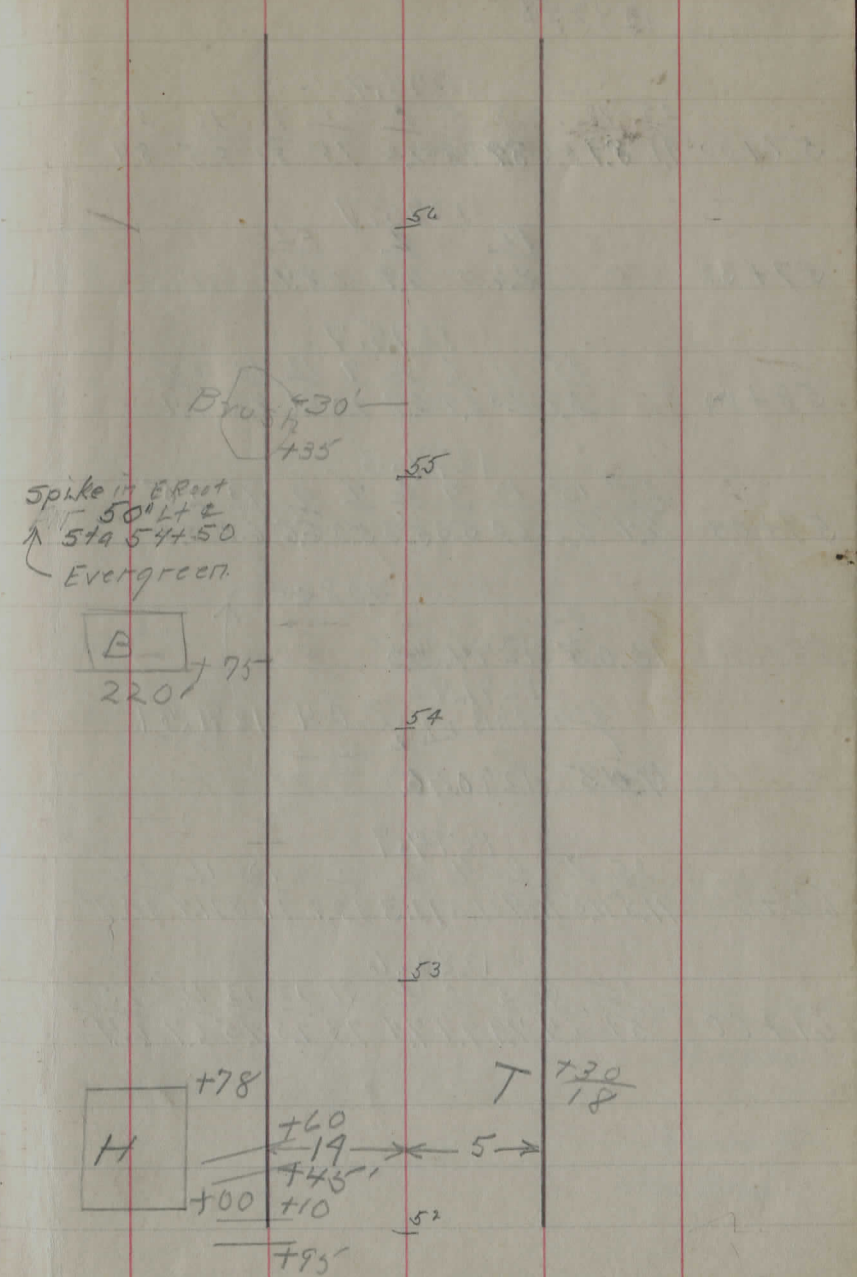
3.94 1278.64

1278.3

55+00	25 / 3.4	17 / 3.6	13 / 4.8	10 / 5.6	9 / 4.6	8 / 4.3	7 / 4.3	9 / 5.2	12 / 4.0	25 / 2.9

1276.3

56+00	25 / 5.8	19 / 6.7	8 / 7.5	7 / 6.8	6 / 6.3	9 / 6.7	11 / 7.5	13 / 7.0	25 / 6.0



1282.58

1275.4

	25	18	10	8	5	2	10	12	16	25
57+00	9.1	8.9	8.4	8.9	7.8	7.2	7.4	8.1	8.5	8.4

1275.7

	FL	2	FL
57+32	8.6	6.9	8.4

1275.7

	25	11	6	2	7	13	18	25
58+00	8.8	8.3	6.9	6.9	7.0	8.1	8.2	8.4

1277.3

	25	15	10	7	2	7	9	13	25
59+00	6.4	6.2	6.0	5.3	5.3	5.3	6.6	6.0	5.8

1.08

13.05 1294.55

1291.92

from this Elev. 3.04 1291.51

9.45 1290.96

1279.7

	25	7	4	4	2	2	10	11	25
60+00	11.5	11.5	11.9	11.3	11.3	10.9	11.8	11.4	10.9

1283.6

	25	9	5	2	2	11	12	13	16	25
61+00	5.1	6.4	7.9	7.4	7.4	7.3	7.8	7.5	6.7	6.4

81.50
13.05
94.55

82.6
81
74.0

61

60

59

BM #7
Spike in Maple
5+a 30' Lt &
5+a 63+50

58

57

7' 11'

+32

12" Sec. C.I.P.
No Good

18"x37.5 Tile
w/Hdwl Good

0.70

4.80 1295.05

1289.3

	150	100	50	25	℄	16	50	100	150
62+00	6.4	6.2	5.0	3.8	5.8	5.9	9.2	11.2	12.3

1290.3

	25	15	12	8	℄	9	19	25
63+00	4.7	5.1	5.3	5.1	4.8	5.1	6.4	6.1

1288.2

	25	21	17	10	8	℄	9	14	25
64+00	6.0	6.2	7.2	7.6	7.4	6.9	7.0	7.7	8.0

1287.5

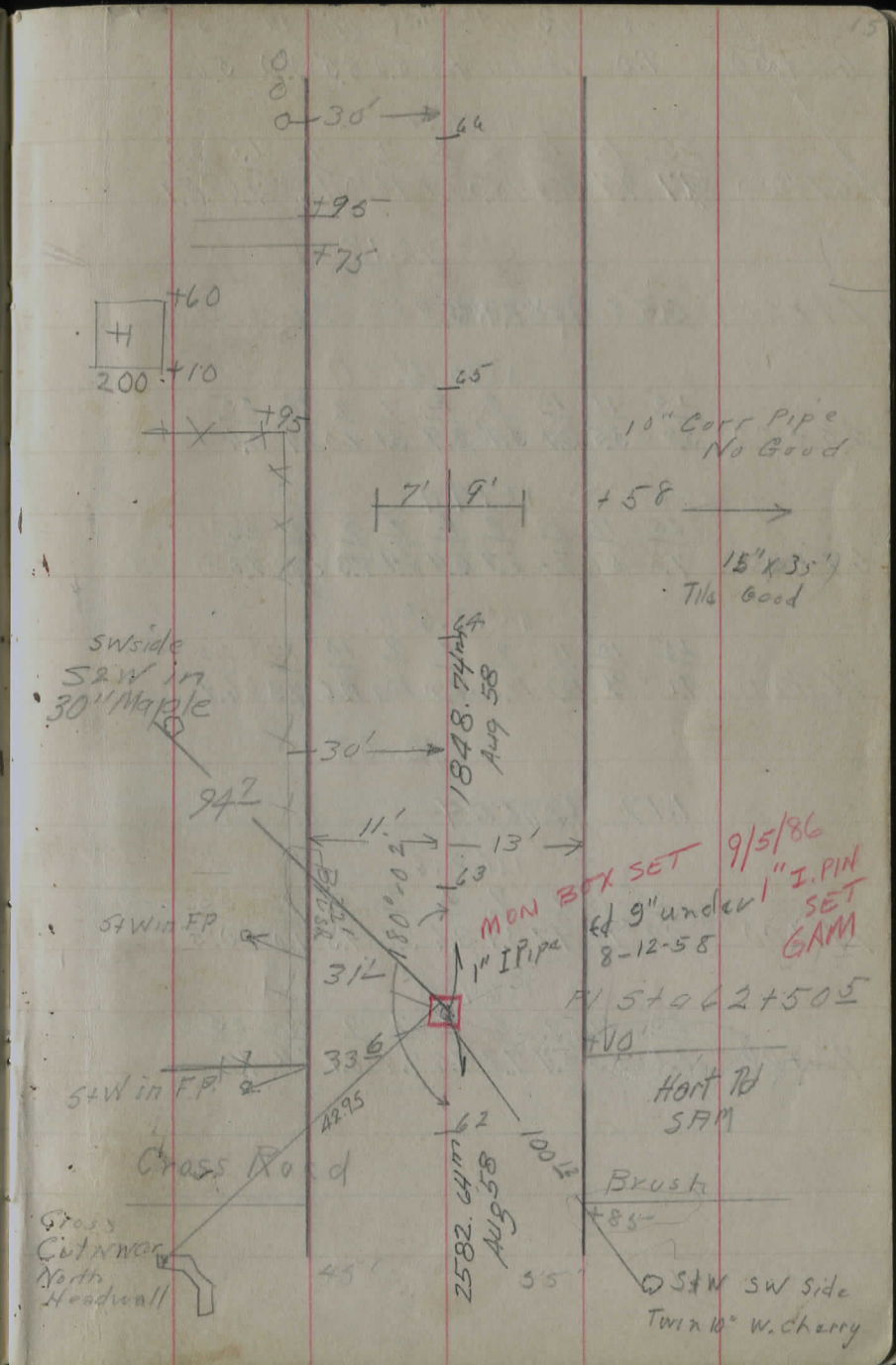
	FL		℄		FL
64+58	8.6		7.4		6.8

1286.8

	25	13	9	6	℄	10	16	25
65+00	7.9	8.1	8.3	8.1	8.2	8.1	9.0	9.0

1287.0

	25	8	℄	I	10	13	25
66+00	9.3	8.4	8.1	7.9	8.2	7.7	6.9



66+50	25	13	11	12	13	6	9	14	20
	9.0	8.2	8.6	7.8	8.0	8.5	7.0	5.6	

1285.12

67+00	25	15	10	6	2	7	9	15	25
	9.7	9.4	10.6	10.3	9.9	10.0	10.8	7.4	5.9

12.18

0.58)283.45

1280.6

68+00	25	11	10	8	2	7	9	12	25
	3.8	3.5	3.9	3.4	2.9	3.1	4.0	2.9	0.6

1277.1

69+00	25	13	10	8	2	7	9	13	25
	7.3	6.7	7.2	6.7	6.4	6.4	7.3	5.8	4.3

1273.5

70+00	25	10	10	8	2	7	10	17	25
	9.1	8.4	10.9	10.3	10.0	10.1	11.6	7.3	6.4

12.38

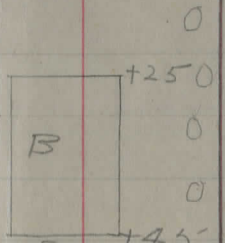
1.17)1272.24

1268.6

71+00	25	15	10	7	4	7	9	16	25
	0.9	1.8	4.7	3.9	3.6	3.6	4.5	1.0	0.5

1264.6

72+00	25	14	9	6	2	7	9	14	25
	8.1	7.3	8.4	7.8	7.6	7.4	8.4	6.4	4.8



71

70

69

68

67

1261.8

	25	11	8	8	8	9	11	13	25
73+00	11.2	10.6	10.9	10.8	10.4	10.0	10.5	9.8	8.7

1259.8

	25	13	9	8	6	4	4	10	12	14	16	25
74+00	14.0	13.4	12.7	12.8	12.6	12.4	12.2	11.8	12.7	12.4	13.0	12.5

11.20

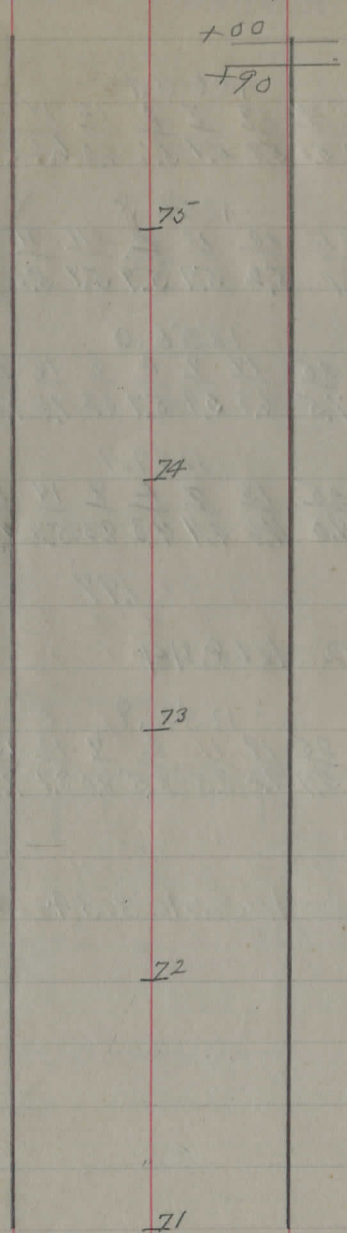
0.65 1261.69

1258.5

	25	15										
	4.6	4.3	14	11	10	8	4	5	6	8	11	14	25
75+00			4.2	3.6	3.6	3.1	3.2	3.0	3.1	2.6	3.5	3.0	3.0

1257.3

	25	12	10	8	6	9	20	26
76+00	5.0	4.6	4.8	4.3	4.4	4.3	4.7	3.0



1261.69

1256.1

	25	15	11	9	7	8	12	14	17	25
77+00	7.5	7.0	6.8	5.8	6.4	5.6	6.0	6.6	6.1	5.5

1255.8

	FL	10	10	8	11	11	FL
77+57	10.1	5.2	5.9	5.9	5.7	6.0	9.9

1256.0

	25	14	7	8	9	16	19	25
78+00	7.5	6.8	5.9	5.7	6.3	7.6	7.2	7.6

1257.4

	25	13	9	8	8	14	18	25
79+00	4.0	4.6	4.4	4.3	4.3	5.3	4.6	3.5

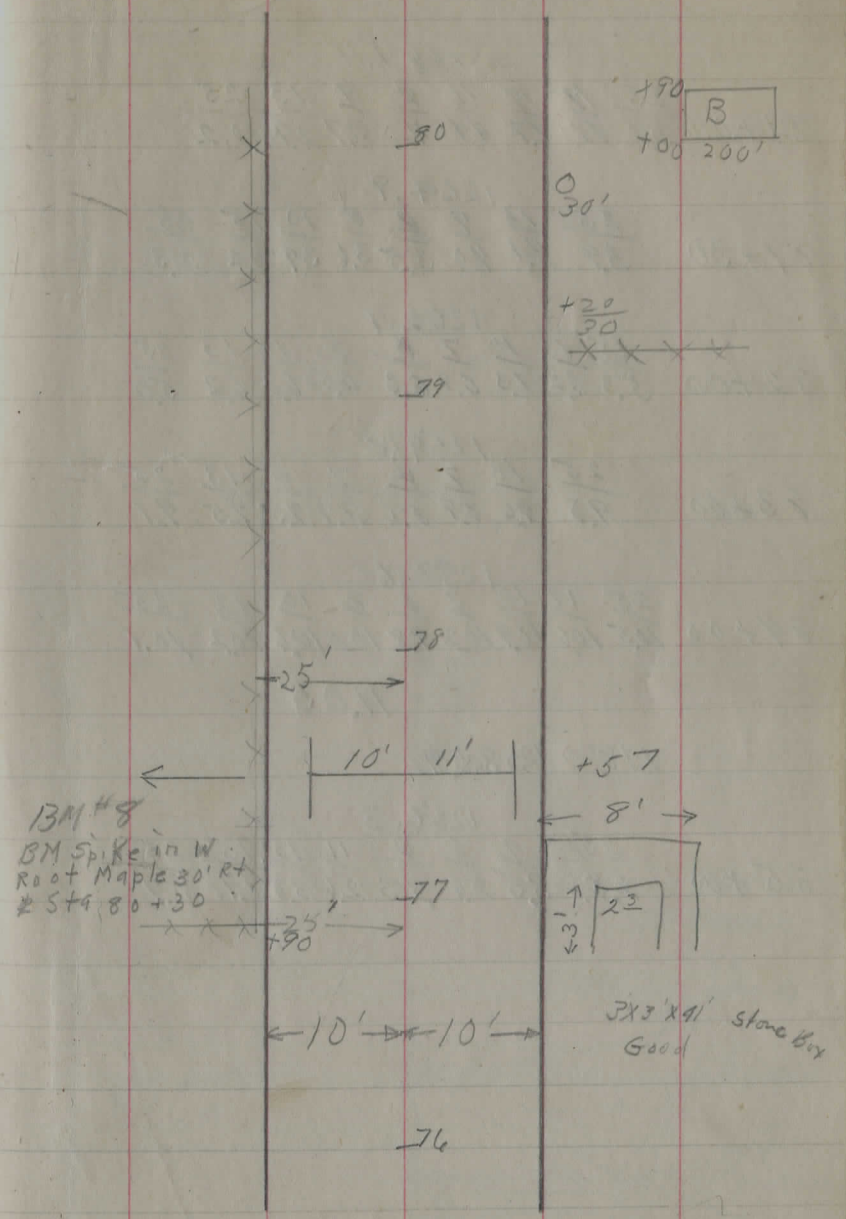
1.97

8.72 1268.44

1259.9

	25	14	11	8	7	10	15	25
80+00	5.9	9.2	8.5	8.5	8.0	8.7	7.2	5.9

3.34 1265.10



1268.44

1264.4

81+00 — 25/3.4 | 19/4.1 | 14/4.7 | 11/4.4 | 8/4.0 | 9/3.7 | 13/2.9 | 25/2.2

1264.9

81+30 — 25/3.9 | 12/4.1 | 9/4.0 | 8/3.5 | 5/3.6 | 10/3.9 | 15/3.2 | 25/2.3

1262.1

82+00 — 25/5.3 | 13/6.2 | 10/7.3 | 7/6.8 | 6/6.3 | 8/6.5 | 11/6.8 | 13/6.2 | 25/5.0

1259.8

83+00 — 25/9.8 | 13/9.4 | 7/8.9 | 6/8.6 | 7/8.9 | 8/9.5 | 13/9.5 | 25/9.1

1258.6

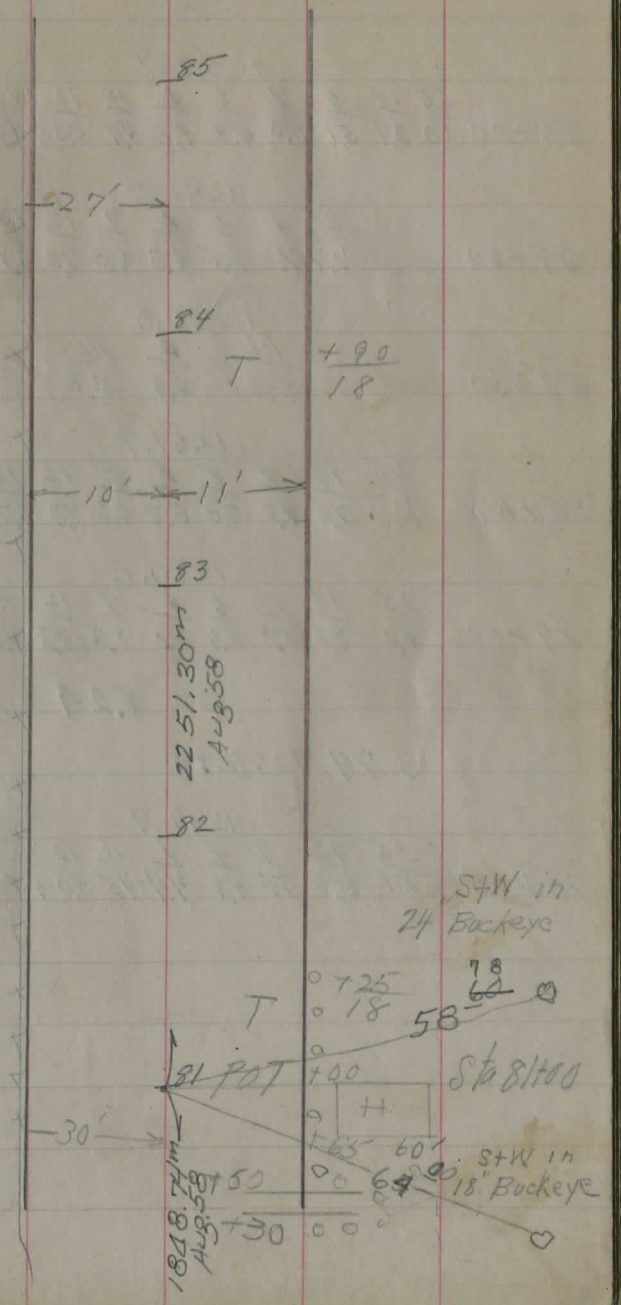
84+00 — 25/10.5 | 17/10.6 | 10/10.9 | 7/10.7 | 6/9.8 | 8/10.0 | 10/10.6 | 12/10.2 | 25/10.1

11.03

L18 1258.59

1256.3

85+00 — 25/1.8 | 9/3.5 | 6/2.6 | 6/2.3 | 11/2.6 | 13/3.3 | 15/1.7 | 25/0.7



1258.59

1253.9

	25	17	9	7	6	6	10	13	14	25
86+00	3.0	3.9	5.1	5.3	4.8	4.7	4.9	5.3	4.9	5.0

1252.3

	25	11	4	4	9	12	13	25
87+00	7.7	7.2	6.5	6.3	6.3	7.2	6.9	6.4

1252.10

	FL	E	FL
87+30	8.3	6.4	8.3

1251.9

	25	12	8	5	4	8	12	16	25
88+00	7.6	7.4	8.0	7.0	6.7	6.6	7.3	6.7	6.3

1250.6

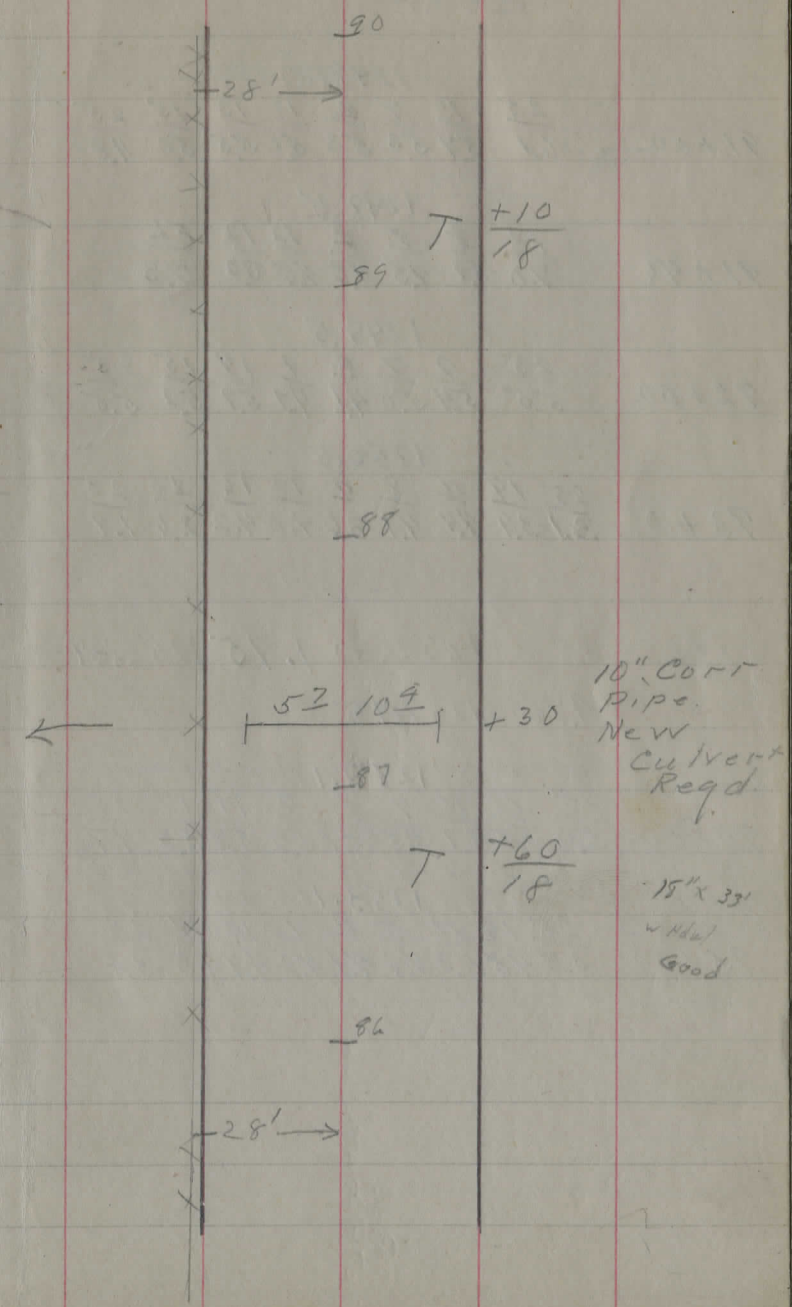
	25	13	10	6	6	9	12	15	25
89+00	8.0	8.2	8.8	8.4	8.0	8.2	8.8	7.9	7.2

8.24

3.79 1254.14

1249.7

	25	12	9	4	4	10	12	15	25
90+00	5.1	5.0	5.5	4.8	4.4	4.5	5.0	4.5	4.2



1254.14

1248.8

91+00	25 / 6.1	13 / 5.7	7 / 5.3	4 / 5.3	10 / 5.1	13 / 5.5	10 / 5.0	25 / 4.8

1249.5

91+46	FL / 7.0	8 / 3.1	5 / 4.5	4 / 4.6	12 / 4.5	12 / 3.2	FL / 7.3	

1249.5

92+00	25 / 5.5	9 / 5.4	7 / 5.0	4 / 4.6	9 / 4.7	14 / 5.7	15 / 5.2	25 / 5.5

1250.5

93+00	25 / 3.1	14 / 3.9	11 / 4.4	8 / 4.1	9 / 3.6	12 / 4.0	14 / 4.2	20 / 2.6	25 / 1.9

1.75 1252.39

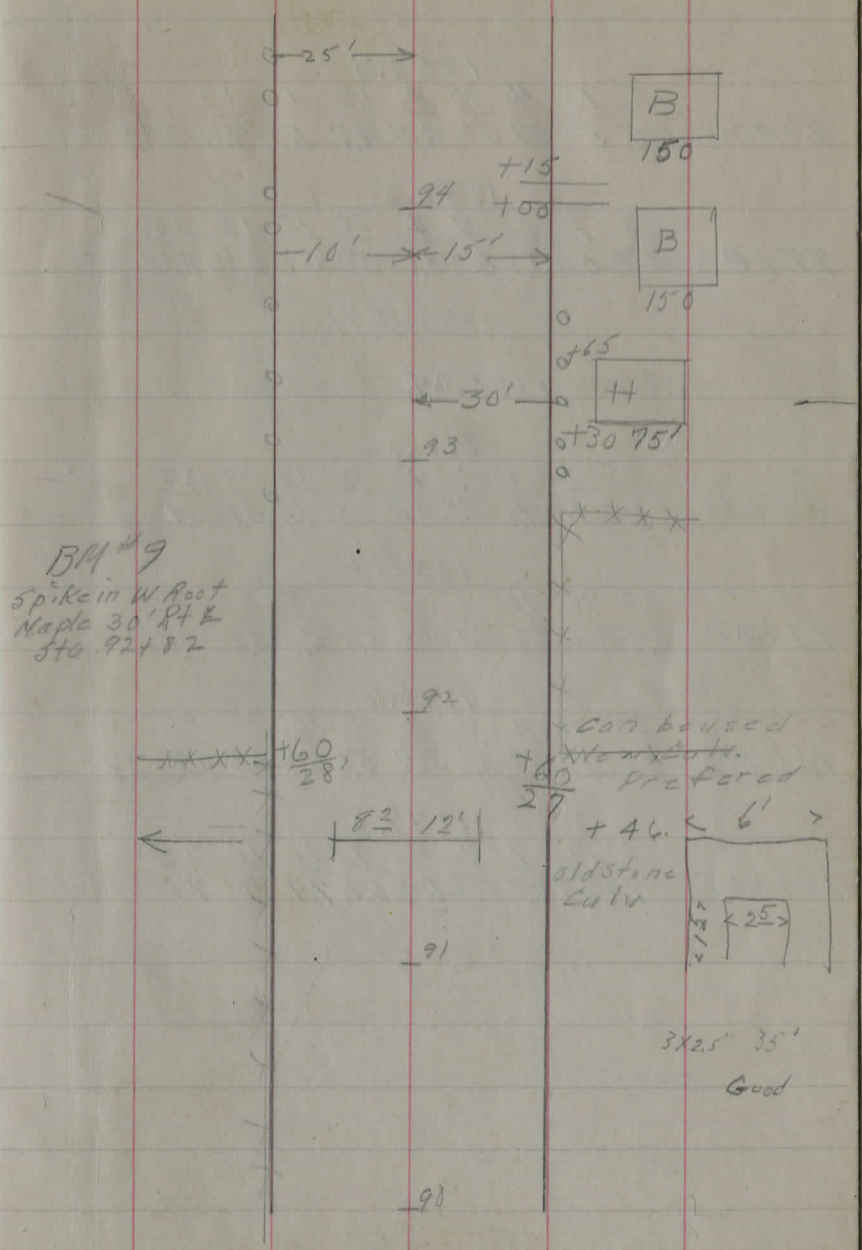
4.76 1257.15

1252.1

94+00	25 / 5.0	13 / 5.5	11 / 6.1	7 / 5.5	6 / 5.1	9 / 5.2	14 / 5.8	17 / 5.3	25 / 4.9

1253.1

95+00	25 / 3.8	14 / 4.5	11 / 5.3	8 / 4.6	6 / 4.1	9 / 4.2	14 / 4.9	17 / 4.3	25 / 3.4



1257.15

1252.5

96+00	25	13	11	10	8	10	15	18	25
	5.5	5.4	5.8	5.0	4.7	4.7	5.3	4.6	3.8

1252.2

97+00	25	12	10	7	4	10	13	18	25
	5.7	5.6	5.8	5.3	5.0	5.0	5.7	5.1	4.7

5.71

4.60 1256.04

1252.2

98+00	25	13	10	7	4	9	13	17	25
	3.8	4.3	4.6	4.1	3.8	3.8	4.5	4.1	3.8

1252.4

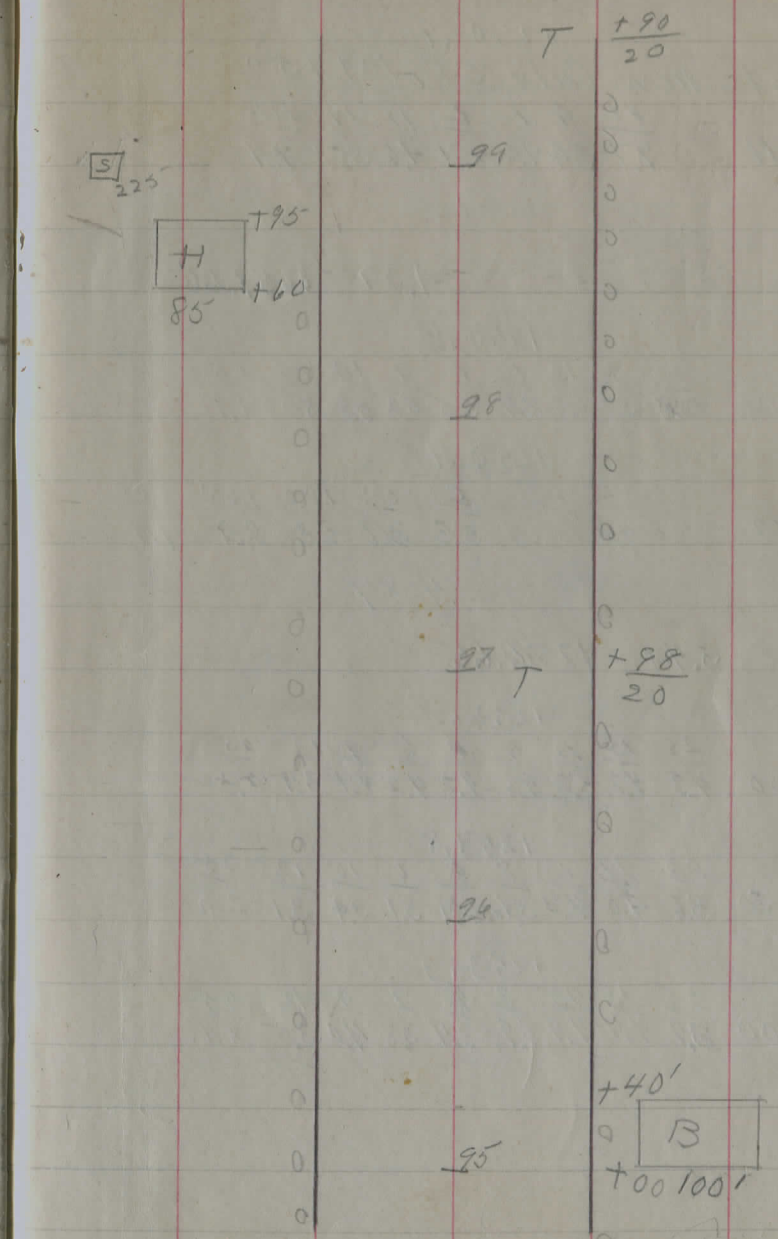
99+00	25	14	11	7	4	11	18	20	25
	3.4	4.0	4.5	4.0	3.6	3.8	5.2	3.8	3.2

1250.6

100+00	25	14	11	8	4	12	15	16	21	25
	4.9	5.1	5.9	5.6	5.4	5.6	6.2	5.8	4.2	3.7

1249.0

101+00	25	13	9	7	4	9	16	17	25
	7.0	6.7	6.7	6.3	6.0	6.1	7.4	7.0	7.0



1256.04

1250.9

Locate new Culv Sta 101+50

	FL	9	9	8	11	11	FL
101+41	7.7	3.4	4.6	5.1	4.6	3.7	8.4

4.39 1251.65

1250.5

	25	14	13	10	8	9	14	18	25
102+00	5.8	5.2	6.0	5.7	5.5	5.2	5.8	5.0	4.9

1250.7

	8	50	100	150	200
102+42	5.3	3.9	2.8	2.4	1.9

4.87

5.48 1256.65

1252.5

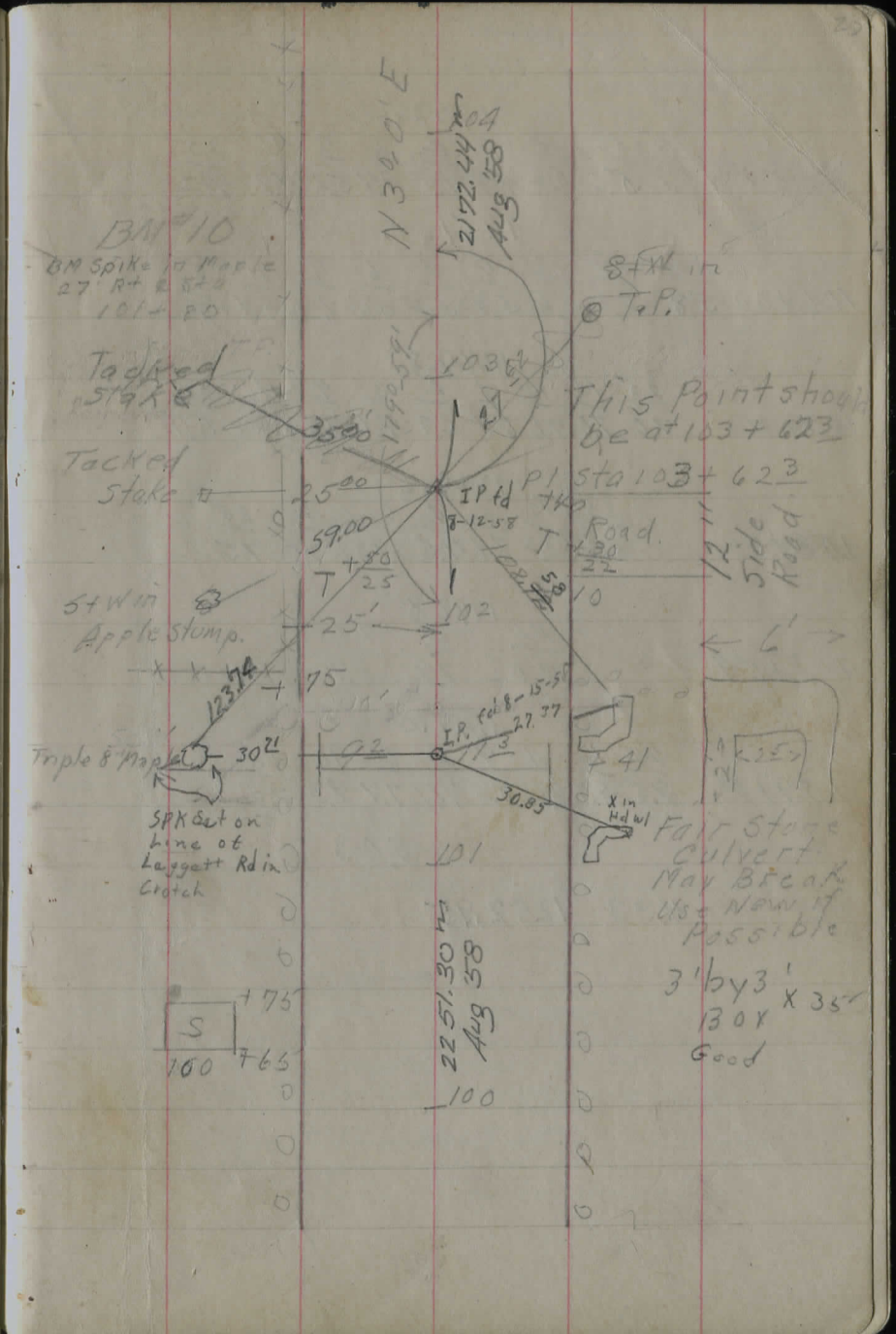
	25	15	12	9	8	6	9	12	25
103+00	4.3	4.6	5.2	4.6	4.2	4.2	4.4	3.9	2.2

1253.8

	25	14	12	8	8	6	10	13	25
103+50	3.6	4.0	4.3	3.6	2.9	3.1	3.4	3.1	2.0

1253.3

	25	16	13	8	8	7	9	11	25
104+00	3.9	4.4	4.9	3.9	3.4	3.8	4.0	3.5	2.9



1256.65

1252.2

	25	16	12	8	4	6	9	11	25
105+00	5.2	5.6	5.8	4.8	4.5	4.7	5.2	4.8	4.2

1251.5

	25	14	12	9	4	6	9	11	25
106+00	5.8	6.2	6.4	5.9	5.2	5.6	6.0	5.4	5.0

1249.8

	25	13	12	9	4	3	9	11	25
107+00	7.0	7.6	7.6	7.4	6.9	7.1	7.2	6.9	5.7

1249.2

	25	12	8	4	6	7	9	25
108+00	8.5	8.2	7.4	7.5	7.7	8.2	7.8	7.5

1248.8

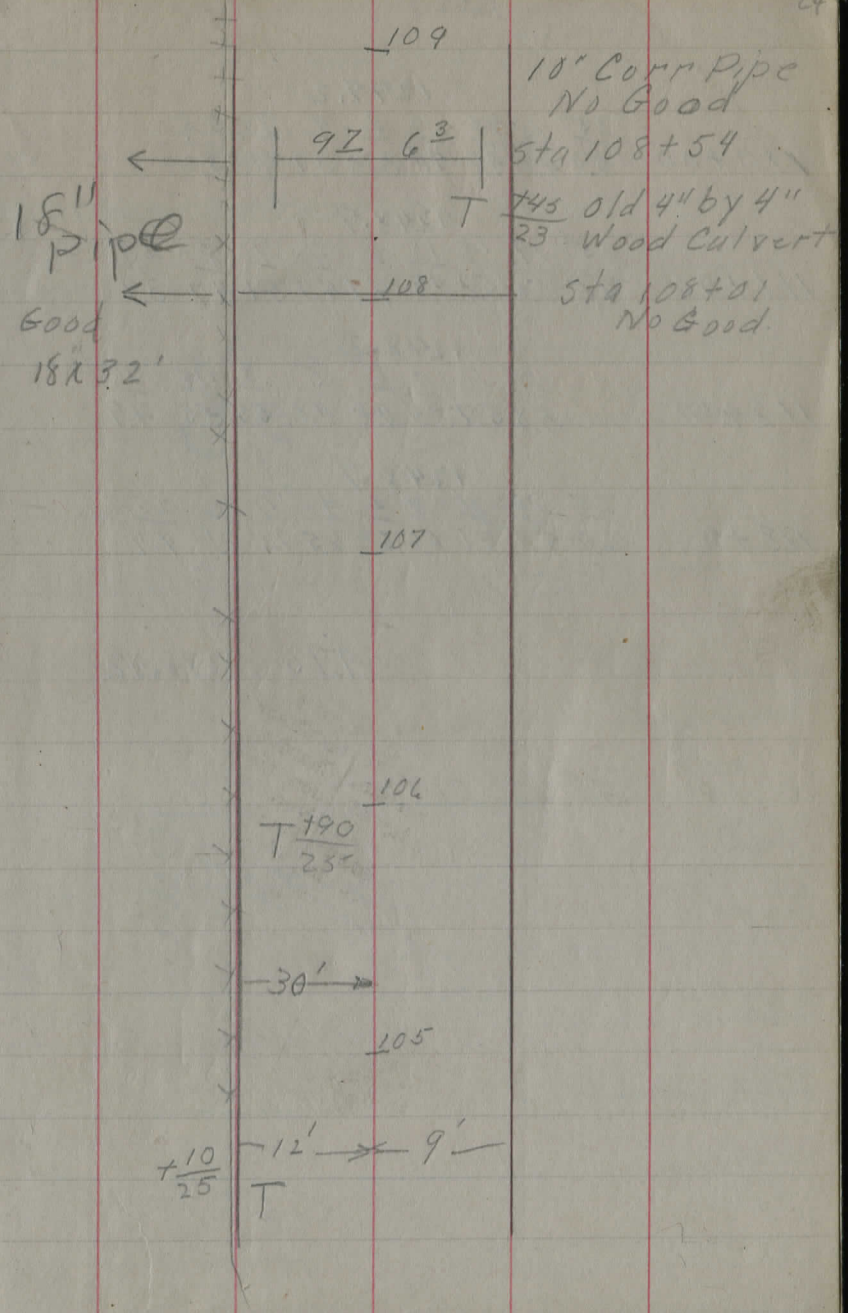
	FL	4	FL
108+54	7.0	7.9	8.7

1249.0

	25	12	11	9	4	6	11	25
109+00	8.5	8.4	8.6	8.2	7.7	7.7	8.3	7.5

8.03

4.33 1252.95



1252.95

1248.2

	25	15	14	10	8	4	9	25
110+00	5.0	4.8	4.9	4.4	3.8	3.9	4.1	3.2

1248.9

	25	19	15	10	8	4	7	8	25
111+00	4.5	5.0	5.2	4.8	4.1	4.4	5.1	4.7	3.7

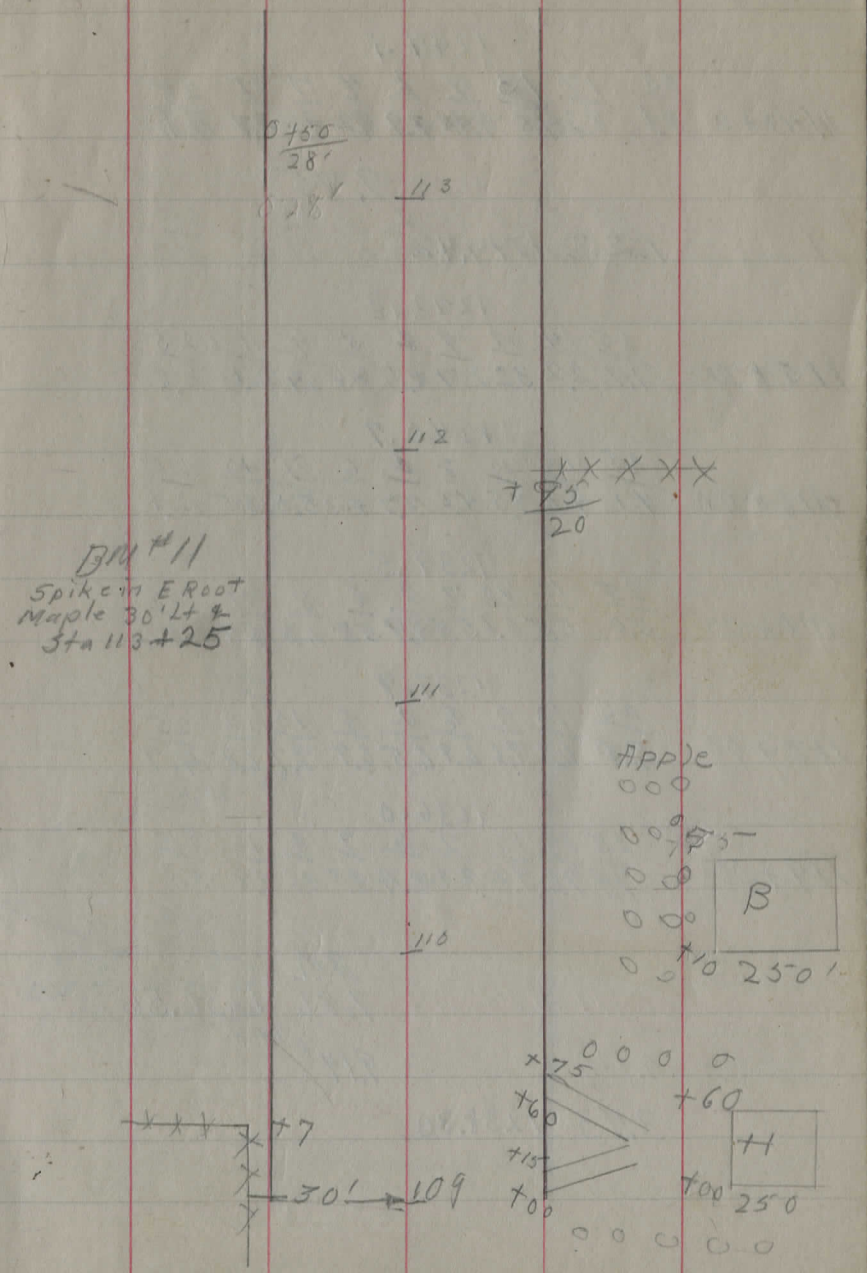
1248.2

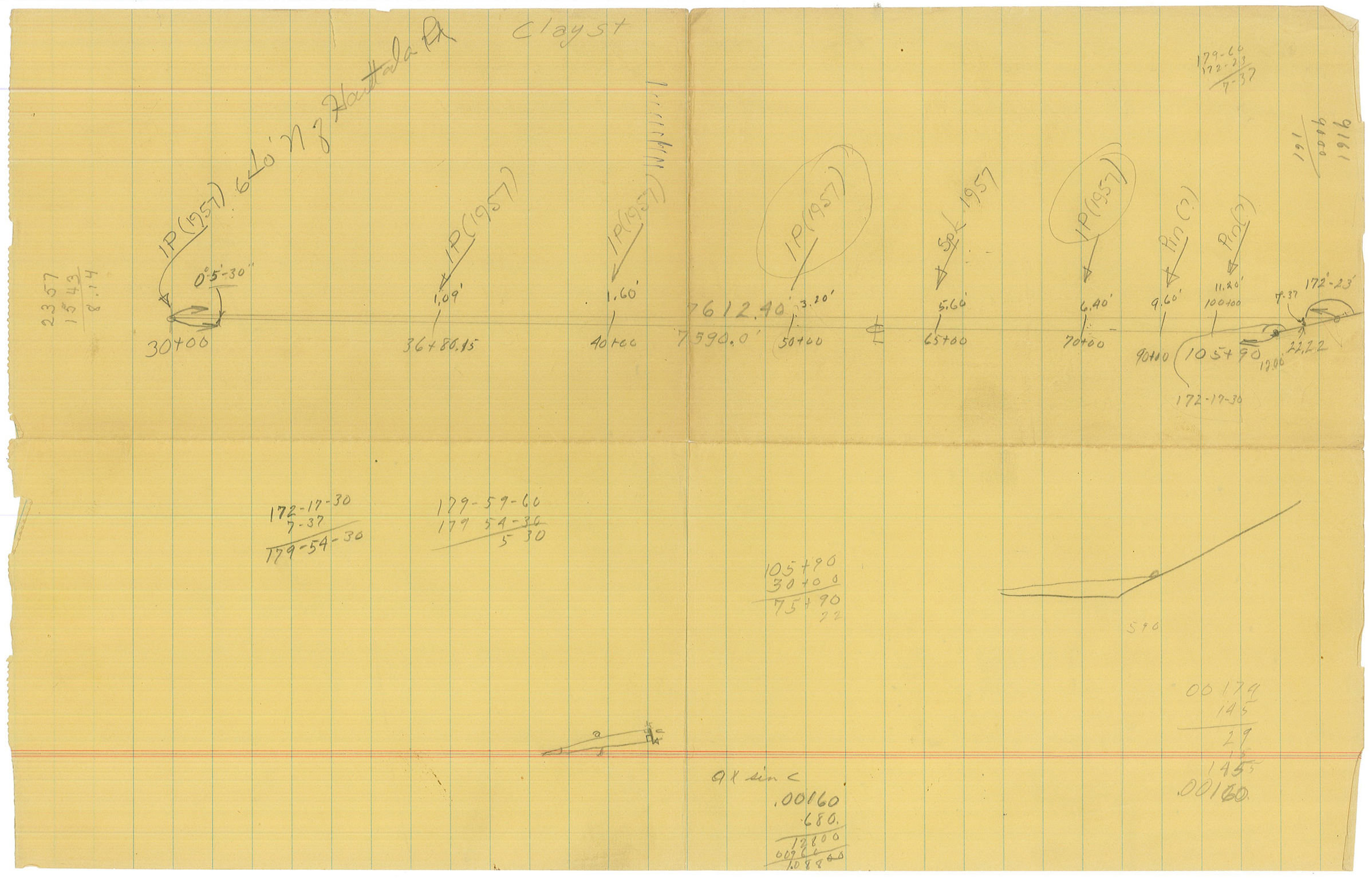
	25	12	9	8	5	8	14	25
112+00	5.8	5.7	5.4	4.8	4.8	5.5	5.5	4.9

1246.7

	25	16	11	8	8	4	7	10	25
113+00	6.0	6.4	7.1	6.6	6.3	6.5	7.1	6.1	4.9

4.93 1248.02




Clay St
Hartala Pl
IP(1957)
0°5'-30"
1.09'
1.60'
7612.40'
3.10'
7590.0'
SPK 1957
5.60'
6.40'
9.60'
11.20'
7-37
172-23'
30+00
36+80.15
40+00
50+00
65+00
70+00
90+00
100+00
105+90
12.00
22.22
172-17-30
179-59-60
179 54-30
5 30
105+90
30+00
75+90
22
590
9 x sin <
.00160
680.
12800
9600
1.0880
00179
145
29
145
.00160

1252.95

1244.1

114+00	25/8.1	17/8.2	13/9.6	7/9.4	4/8.9	4/8.2	7/9.8	11/9.7	25/7.1

9.75

1.22 1244.42

1242.3

115+00	25/1.4	14/2.2	11/3.2	9/2.7	4/2.1	5/2.6	7/3.4	11/2.1	25/0.8

1240.7

116+00	25/4.1	12/4.1	10/4.5	8/4.2	4/3.7	6/4.3	7/5.0	10/3.5	25/2.1

1239.5

117+00	25/5.0	12/5.5	10/6.1	7/5.5	4/4.9	6/5.8	8/6.3	11/6.4	25/3.6

1237.9

118+00	25/7.0	13/6.8	9/7.6	6/6.9	4/6.5	6/6.9	10/7.7	12/6.8	25/4.7

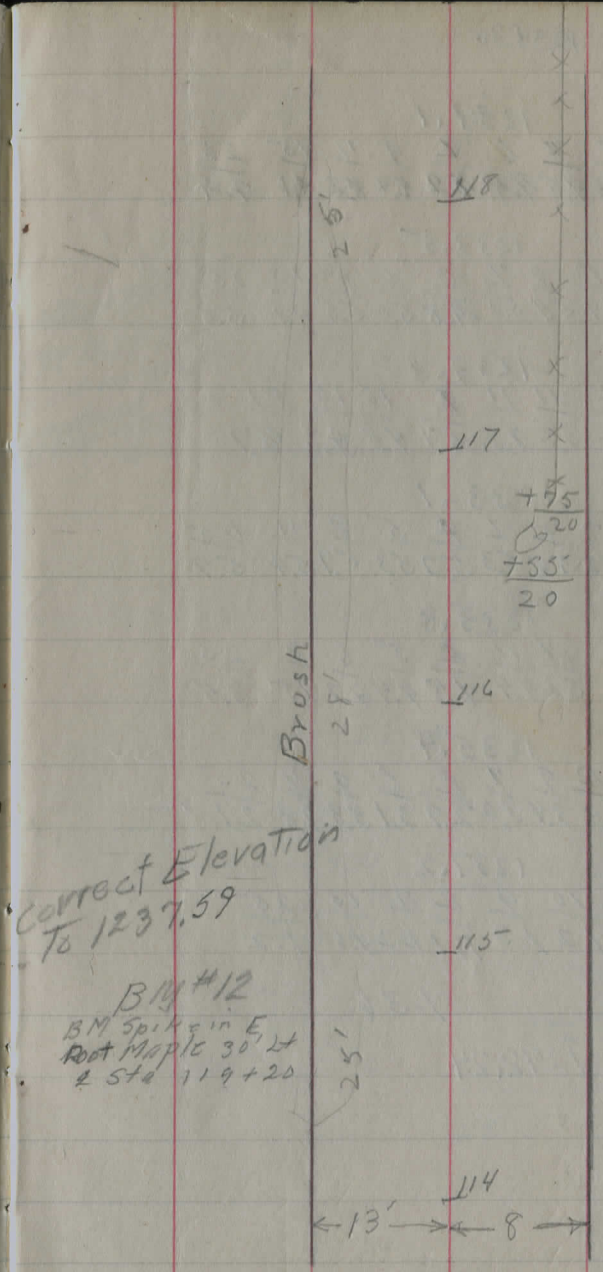
1236.0

119+00	25/7.9	19/7.6	10/9.2	7/8.7	4/8.4	7/8.8	9/9.6	12/8.8	25/5.3

BM 7.86 1236.56

9.14 ← Turn

3.43 1238.30

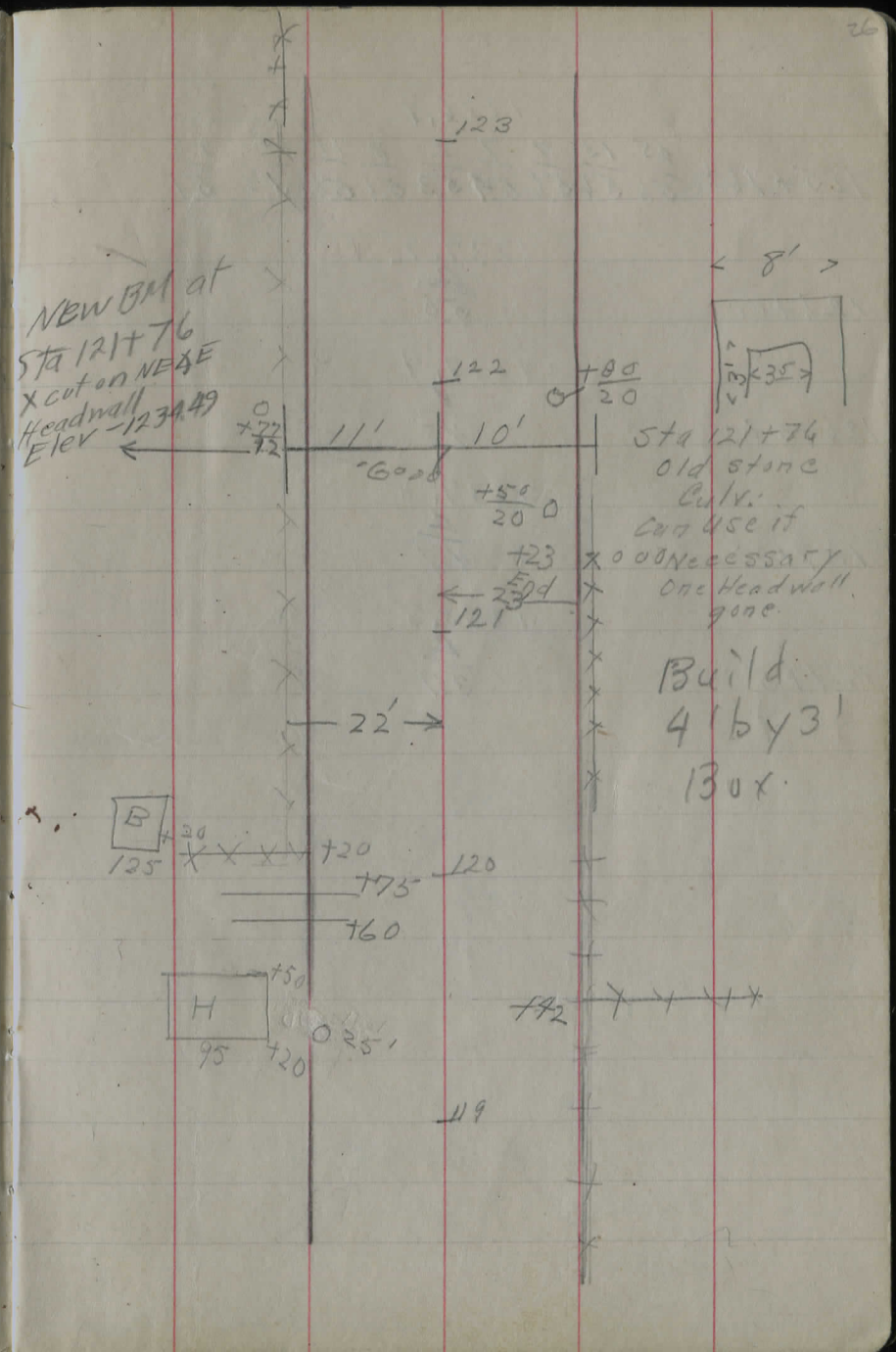


1238.30

		1234.1							
	25	9	7	6	8	9	11	15	25
120+00	4.3	4.2	4.5	4.4	4.2	4.4	4.2	4.1	4.4
		1233.5							
	25	10	9	7	8	6	8	10	25
121+00	5.4	4.9	5.4	5.0	4.8	5.0	5.5	4.9	5.8
		1233.2							
	FL	11	11	8		10	10	FL	
121+76	9.0	8.9	4.8	5.1		4.8	4.2	8.7	
		1233.1							
	25	10	8	7	8	5	8	11	25
122+00	5.9	5.2	5.6	5.3	5.2	5.3	6.9	5.4	5.7
		1233.8							
	25	14	11	8		5	6	8	25
123+00	5.1	5.1	4.9	4.5		4.4	4.7	4.5	3.4
		1235.4							
	25	12	9	7	8	6	9	11	25
124+00	2.1	3.0	3.4	3.0	2.9	3.1	3.3	2.8	2.1
		1237.2							
	25	11	10	9	8	7	13	25	
125+00	1.6	1.6	1.2	1.3	1.1	1.2	1.6	1.2	

1.36

5.71 1242.24



1236.9

125+76 — 25/5.6 13/5.6 11/5.6 7/5.4 2/5.3 8/5.1 11/6.8 15/5.2 20/5.1

1237.2

126+00 — 6/5.0

1237.4

126+50 — 4/4.8

1237.8

127+00 — 4/4.4

1238.5

127+50 — 6/3.7

125 35
121 76
3 59

Δ 9°-50

D = 3°-30'

E = 6.04

T = 140.83

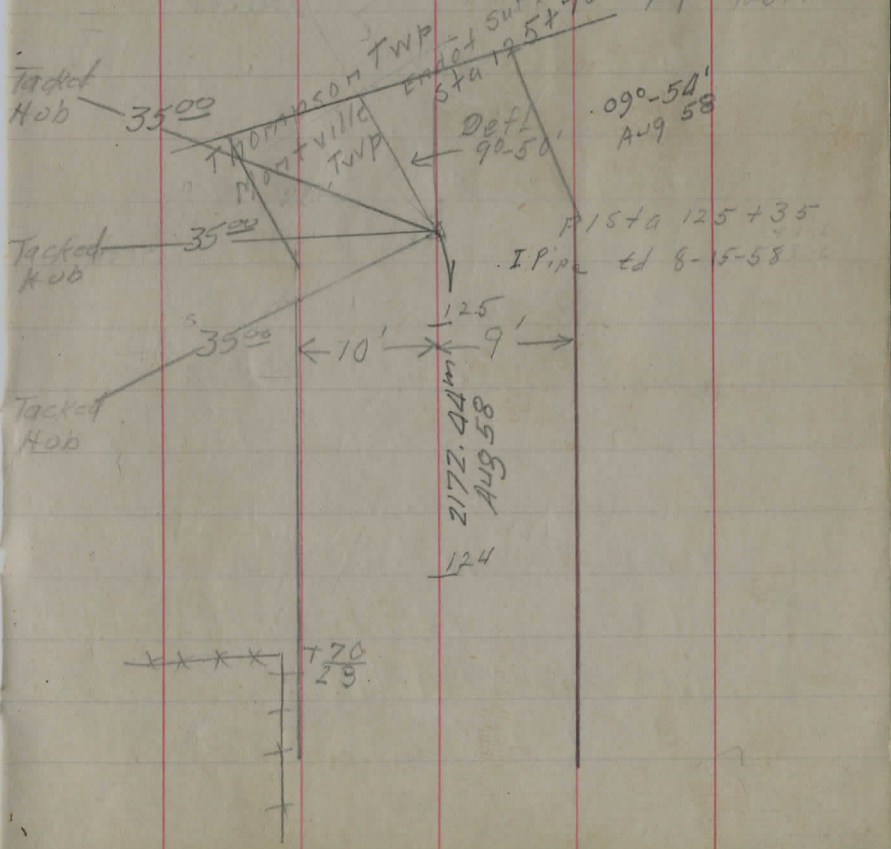
L = 280.95

PC = 123+94 17

PI = 125+35

PT = 126+75 12

See B 72 for continuation



		1280.73				
57			4.40	1276.33	F2.5 / 22.7	F1.8 / 23.1
	6.04	1283.11	3.66	1277.07		
58			6.43	1276.68	F2.6 / 22.1	F2.2 / 23.0
59			4.58	1278.53	F2.3 / 22.9	F1.9 / 23.3
60				1281.67	23.0	23.4

Check Levels

Elv. P.V.C. inside edge on ℄ Road	1264.15			
7.83				
	6.64	1265.34	B.M. W.W. Cor Headwall Sta 0+00	
	1.07			
11.09	1282.90			
	0.23			
9.12	1290.89			
	0.51			
11.69	1302.07			
	0.33			
6.53	1308.27			#1 B.M. Sta. 13+00
	5.17	1303.10		
	6.43			
0.60	1302.44			
	11.85			
1.45	1292.04			#2 B.M. Sta 23+92
	4.89	1287.15		
	4.95			#3 B.M. Sta. 30+50
9.38	1296.47			
	2.26	1294.21		
5.72	1299.93			
	0.36			#4 B.M. Sta 32+85
7.10	1306.67			
	6.44	1300.23		
	10.09			
0.51	1297.09			
	9.66			#5 B.M. Sta 47+90
0.32	1287.75			
	10.94	1276.81		
	11.11			
0.72	1277.36			
	2.46			#6 B.M. Sta. 54+50
8.48	1283.38			
	4.77	1278.61		
	2.46			

1224	1293.16			#7 B.M. Sta 63+50
		1.63	1291.53	
0.50	1292.03			
		13.03		
0.96	1279.96			
		12.16		
1.16	1268.96			#8 B.M. Sta 80+30
		3.84	1265.12	
		12.64		
0.60	1256.92			#9 B.M. Sta 92+82
		4.55	1252.37	
		4.24		
4.65	1257.33			#10 B.M. Sta 101+85
		5.64	1251.69	
		8.33		
0.63	1249.63			#11 B.M. Sta 113+25
		1.59	1248.04	
		10.98	1238.65	#12 B.M. Sta 119+20
1.08	1239.73	3.21	1236.52	

New BM at Sta 121+76 on NE A Headwall
Xcut on NE A
Elev — 1234.49

Correct Elevation is 1237.59

Sta	BS	HI	Grade Rod	FS	
BM #12	1.51	1238.03			1236.52
Flow R			9.53		1228.50
Stake R				5.73	C3 8
Flow L			10.03		1228.00
Stake L				6.63	C3.4
BM #11	5.56	1253.60			1248.04
Flow R			5.90		1247.70
Stake R				3.70	C2.2
Flow L			6.40		1247.20
Stake L				4.60	C 1.8
BM #10	5.12	1256.81			1251.69
Flow N			7.21		1249.60
Stake N				3.41	C3.8
Flow S			7.61		1249.20
Stake S				4.91	C 2.7

Sta 121+76

℄

Fl. 1228.0
C. 3.4

Fl. 1228.5
C. 3.8

19' 18'

Sta 108+54

℄

Fl. 1247.2
C. 1.8

Fl. 1247.7
C 2.2

18' 18'

Sta 102+42

Fl 1249.6
C. 3.8

℄

19 5/2

21'

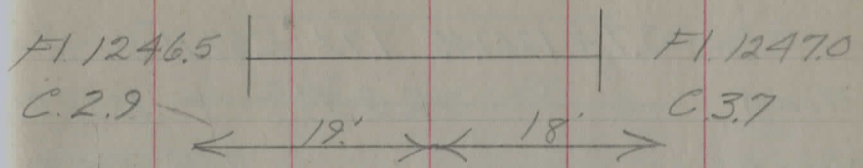
21'

Fl. 1249.2
C. 2.7

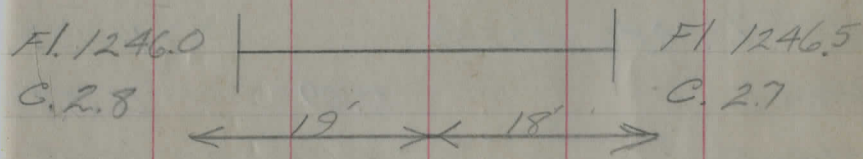
Sta	BS	HI	Grade Rod	FS	
BM #10	4.41	1256.10			1251.69
Flow R			9.10		1247.00
Stake R				5.40	C 3.7
Flow L			9.60		1246.50
Stake L				6.70	C 2.9
BM #9	2.28	1254.65			1252.37
Flow R			8.15		1246.50
Stake R				5.45	C 2.7
Flow L			8.65		1246.00
Stake L				5.85	C 2.8
		7/19/28	Richey Whiskin	Parks Spokn	
B #9	1.81	1254.18			1252.37
Flow R			4.18		1250.00
Stake R				1.28	C 2.9
Flow L			4.68		1249.50
Stake L				2.48	C 2.2

Sta 101+41

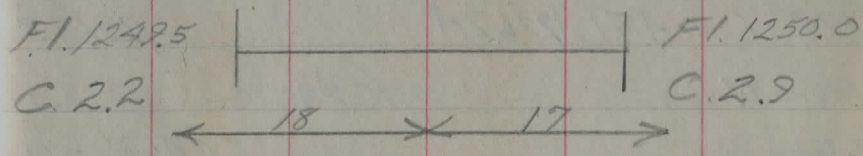
℄



℄ Sta 91+46



℄ Sta 87+30



7/19/28

Sta	BS	HI	Grade Rod	FS	
BM #8	0.38	1265.50			1265.12
	3.74	1261.45	7.79	1257.71	
Flow R			9.95		1251.50
Stake R				7.65	C 2.3
Flow L			10.45		1251.00
Stake L				7.65	C 2.8

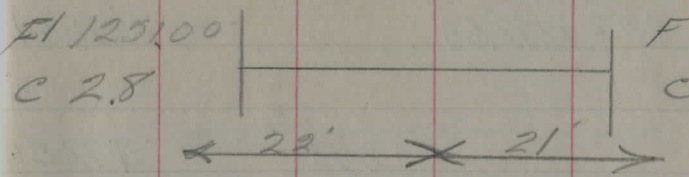
7/19/28

BM #7	0.86	1292.39			1291.53
Flow R			7.09		1285.30
Stake R				6.29	C 0.8
Flow L			6.59		1285.80
Stake L				4.09	C 2.5

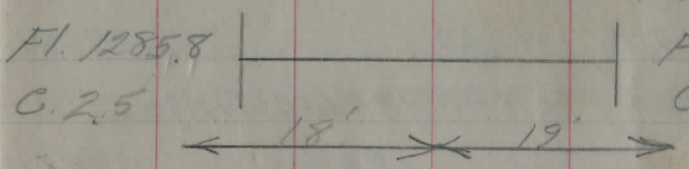
7/19/28

BM #7	4.71	1296.24			1291.53
Flow N			10.94		1285.30
Stake N				5.04	C 5.9
Flow S			12.04		1284.20
Stake S				6.64	C 5.4

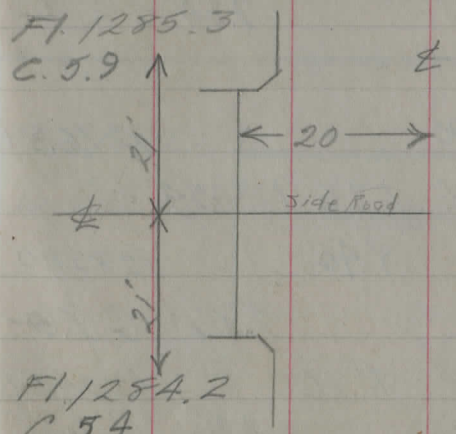
℄ Sta 77+57



℄ Sta 64+58



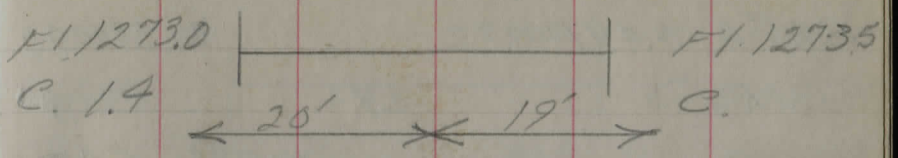
Sta 61+95



7/19/28

	BS	HI	Grade Rod	FS	
BM #6	4.02	1282.63			1278.61
Flow R			9.13		127350
Stake R				7.53	C1.6
Flow L			9.63		127300
Stake L				8.23	C1.4

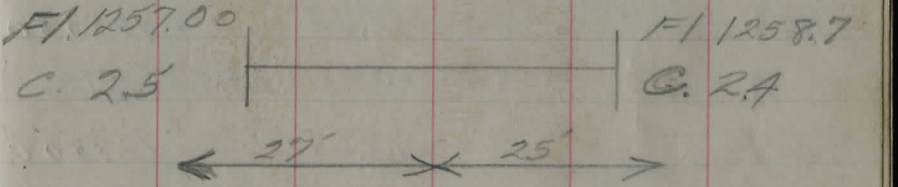
℄ Sta 57+32



7/19/28

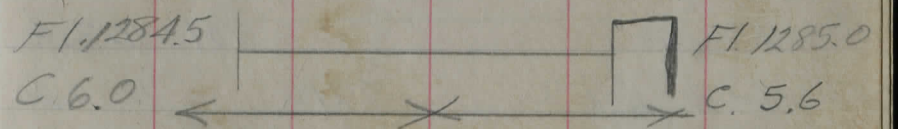
BM #6	1.88	1280.49			1278.61
	2.17	1270.40	12.26	1268.23	
Flow R			13.40		1257.00
Stake R				10.90	C 2.5
Flow L			11.70		1258.70
Stake L				9.30	C 2.4

Sta 50+75



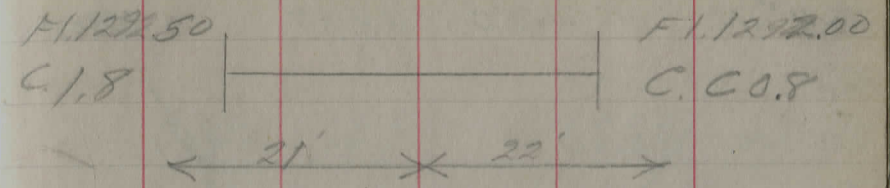
BM #5	9.09	1285.90			1276.81
	8.92	1293.46	1.36	1284.54	
Flow R			8.46		128500
Stake R				2.86	C 5.6
Flow L			8.96		128450
Stake L				2.96	C 6.0

Sta 45+90

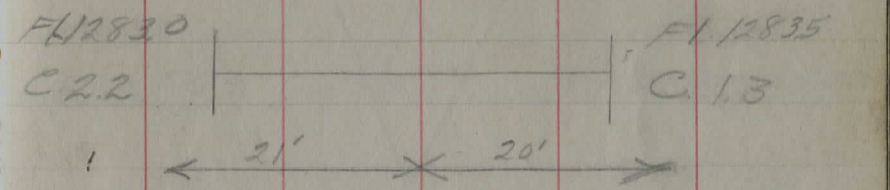


	BS	HI	Grade Rod	FS	
BM#4	0.49	130.72			130.23
Flow R			8.72		122.00
Stake R				7.92	C0.8
Flow L			8.22		122.50
Stake L				6.42	C1.8
BM#3	1.47	125.68			124.21
Flow R			12.18		123.50
Stake R				10.88	C1.3
Flow L			12.68		123.00
Stake L				10.48	C2.2
BM#2	5.26	122.41			117.15
Flow R			7.71		124.70
Stake R				5.31	C2.4
Flow L			8.21		124.20
Stake L				6.51	C2.7

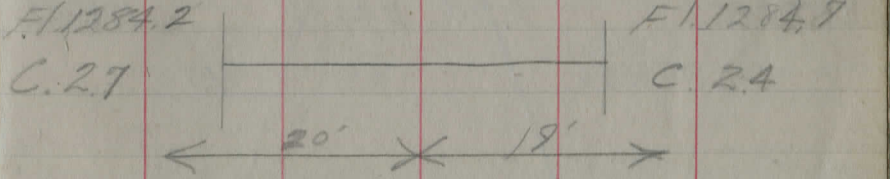
℄ Sta 41+73



Sta 27+61



Sta 23+31



3/6/28

Sta	BS	HI	FS	
BM #12	3.35	239.87		236.52
125+00	236.86		3.01	
124+00	236.02		3.85	
123+00	235.18		4.69	
122+00	234.34		5.53	
121+00	234.13		5.74	
120+00	235.17		4.70	
3/7/28				
BM #12	8.04	244.56		236.52
119	236.86		7.70	
118	238.55		6.01	
117	240.24			

slopes are offset 3 ft.

F0.6 25.1	F0.8 22.1	F0.3 22.9	F0.1 25.9
F0.3 25.3	F0.7 22.3	F0.2 22.0	C0.0 25.0
F2.5 22.5	F2.8 19.5	F1.3 21.4	F1.0 24.4
F2.6 22.4	F2.6 19.4	F2.5 19.6	F2.5 22.6
F1.8 23.3	F2.0 20.3	F2.2 20.0	F2.0 23.0
F1.8 23.5	F1.9 20.5	F1.7 21.5	F1.7 23.8
F1.3 24.4	F1.3 21.4	C1.3 23.2	C1.8 28.2
F2.1 22.9	F2.3 19.9	F0.3 22.9	C0.3 25.9
	21	245	

Sta		BS	9/7/28 HI	Richel Whiskin FS	Parks Snyder
BM #		1.56	1249.60		1248.04
114+00	1245.31			4.29	
115+00	1243.62			5.98	
116+00	1241.93			7.67	
117+00	1242.24			9.36	
		4.63	1244.07	10.16	1239.44
118+00	1238.55			5.52	
119+00	1236.86			7.21	
BM #12				6.48	1237.59
120+00	1235.17			8.90	
121+00	1234.13			9.94	
NW.W. Headwall		7.31	1241.74	9.64	1234.43
122+00	1234.34			7.40	

F0.2 25.6	F0.5 27.6	C0.6 24.2	C0.7 27.2
F1.1 25.3	F0.7 22.3	C0.2 23.6	C0.4 26.6
F1.6 23.9	F1.6 20.9	C0.2 23.6	C0.5 26.6
F0.8 24.8	F0.9 21.8	C0.7 24.3	C0.8 27.3
F1.1 24.5	F1.2 21.5	C0.9 24.6	C1.6 27.6
F0.3 25.9	F0.3 22.9	C2.4 26.8	C3.0 29.2
F0.7 25.1	F0.8 22.1	F0.6 22.4	F0.7 25.4
F0.9 24.8	F0.9 21.8	F1.1 21.7	F1.2 24.7
F1.5 23.9	F1.6 20.9	F1.3 21.4	F1.3 24.4

Sta		BS	HI	FS	
			1141.74		
123+00	1235.18			6.56	
124+00	1236.02			5.72	
125+00	1236.86			4.88	
		9/7/28			
BM #11		5.52	1253.56		1248.04
113+00	1246.77			6.79	
112+00	1247.79			5.77	
111+00	1248.59			4.97	
110+00	1249.38			4.18	
109+00	1250.16			3.40	

F1.6 / 23.8	F1.7 / 20.8	F0.3 / 22.9	C0.2 / 25.9	
C0.7 / 26.7	C0.3 / 23.7	C0.8 / 24.5	C1.2 / 27.5	
C0.4 / 27.2	C0.3 / 24.2	C0.7 / 24.3	C0.9 / 27.3	
C0.4 / 26.6	C0.2 / 23.6	C1.2 / 25.1	C1.4 / 28.1	
F0.6 / 25.3	F0.7 / 22.3	C0.4 / 23.9	C0.5 / 26.9	
F0.3 / 25.6	F0.5 / 22.6	C0.7 / 24.3	C0.7 / 27.3	
F1.2 / 24.2	F1.4 / 21.2	C0.4 / 23.9	C0.3 / 26.9	
F2.1 / 23.3	F2.0 / 20.3	F1.1 / 21.6	F0.8 / 24.6	

STA		BS	HI	FS							
			1253.56								
108+00	1250.25			2.61							
107+00	1251.72			1.84							
		8.28	1257.90	3.94	1249.62						
106+00	1252.48			5.42							
105+00	1253.17			4.73							
104+00	1253.36			4.54							
103+00	1252.93			4.97							
102+00	1252.07			5.83							
BM #10		4.62	1256.31	6.30	1251.69	1251.69					
101+00	1251.58			4.73							
100+00	1251.57			4.74							

F2.6 / 22.4	F2.6 / 19.4	F1.9 / 20.5	F1.9 / 23.5								
F2.1 / 22.7	F2.4 / 19.7	F1.1 / 21.7	F0.7 / 24.7								
F1.8 / 23.5	F1.9 / 20.5	F1.0 / 21.8	F0.9 / 24.8								
F1.6 / 23.6	F1.8 / 20.6	F1.0 / 21.8	F0.7 / 24.8								
F0.4 / 25.1	F0.8 / 22.1	C0.2 / 23.6	C0.4 / 26.6								
F0.4 / 25.6	F0.5 / 22.6	C1.3 / 25.2	C1.5 / 28.2								
F1.7 / 23.5	F1.8 / 20.5	F1.2 / 21.5	F0.9 / 24.5								
F2.1 / 22.7	F2.4 / 19.7	F2.4 / 19.7	F2.5 / 22.7								
F0.3 / 25.6	F0.5 / 22.6	C0.7 / 24.3	C1.2 / 27.3								

Sta		BS	HI	FS	
			1256.31		
99+00	1252.00			4.31	
98+00	1252.50			3.81	
97+00	1253.00			3.31	
		5.96	1257.56	4.71	1251.60
96+00	1253.50			4.06	
95+00	1253.56			4.00	
94+00	1252.70			4.86	
93+00	1251.42			6.14	
		11.9	1253.56	5.14	1252.42
92+00	1250.27			3.29	
91+00	1249.94			3.62	

C0.9 / 27.0	C0.5 / 24.0	C0.8 / 24.5	C1.2 / 27.5
F0.2 / 25.4	F0.6 / 22.4	F0.3 / 22.9	F0.3 / 25.9
F1.4 / 24.1	F1.5 / 21.1	F0.7 / 22.3	F0.4 / 25.3
F1.3 / 23.5	F1.9 / 20.5	F0.5 / 22.6	C0.1 / 25.6
C0.2 / 26.3	C0.0 / 23.3	C0.0 / 23.0	C0.7 / 26.3
F0.5 / 25.4	F0.6 / 22.4	F0.6 / 22.4	F0.1 / 25.4
F0.2 / 25.4	F0.6 / 22.4	F0.1 / 23.2	C0.4 / 26.2
BM #9 1252.37			
F1.7 / 23.8	F1.7 / 20.8	F1.7 / 20.8	F1.7 / 23.8
F1.8 / 23.8	F1.7 / 20.8	F0.7 / 22.3	F0.6 / 25.3

Sta		BS	H.I	FS					
			1253.56						
90+00	1250.43			3.13		F1.3 / 24.2	F1.4 / 21.2	F0.4 / 22.7	F0.4 / 25.7
89+00	1251.06			2.50		F0.2 / 25.6	F0.5 / 22.6	C0.4 / 23.4	C0.4 / 26.4
88+00	1251.77			1.79		F0.8 / 25.0	F0.9 / 22.0	C0.3 / 23.7	C0.6 / 26.7
				0.20	1253.36	NW Cor W. Headwall T.P			
87+00	1253.08					—	20.0	21.5	—

9/9/28

Sta		BS	HI	FS	
TP		8.92	1262.28		1253.36
87+00	1253.08			9.20	
86+00	1255.00			7.28	
85+00	1257.00			5.28	
84+00	1259.00			3.28	
83+00	1261.00			1.28	
		10.59	1269.38	3.49	1258.79
82+00	1262.76			6.62	
81+00	1262.84			6.54	
BM #8		4.38	1269.50	4.38	1265.00
80+00	1261.24			8.26	
79+00	1259.40			10.10	
		3.79	1261.89	11.40	1258.10

F2.0 / 23.3	F2.0 / 20.3	F0.7 / 22.0	F0.8 / 25.0	1265.12
C0.7 / 26.7	C0.3 / 23.7	F1.4 / 21.2	F1.3 / 24.2	
C1.0 / 26.2	C1.3 / 25.2	C1.1 / 24.9	C1.4 / 27.2	
F0.8 / 24.7	F1.1 / 21.7	F0.8 / 22.1	F0.8 / 25.1	
F2.2 / 22.6	F2.5 / 19.6	F1.9 / 20.5	F1.7 / 23.5	
C0.5 / 26.6	C0.2 / 23.6	C0.2 / 23.6	C0.6 / 26.6	
C2.1 / 29.0	C1.8 / 26.0	C3.4 / 28.4	C3.8 / 31.4	
C1.4 / 28.4	C1.4 / 25.4	C2.3 / 26.7	C2.3 / 29.7	
F1.6 / 23.3	F2.0 / 20.3	F2.2 / 20.0	F1.3 / 23.0	

Sta		BS	HI	FS	
			126.89		
78+00	125.98			3.91	
77+00	125.37			4.52	
76+00	125.58			4.31	
75+00	125.72			3.17	
74+00	126.54			1.35	
		12.00	127.54	3.35	125.54
73+00	126.18			7.36	
72+00	126.64			3.90	
		12.50	128.88	0.16	127.38
71+00	127.52			12.36	
70+00	127.40			8.48	

F3.6 24.1	F3.6 21.1	F3.7 21.3	F3.8 24.3
F2.8 22.5	F2.8 19.5	F1.9 20.5	F1.0 23.5
F1.0 25.1	F0.8 22.1	C1.0 24.8	C1.6 27.8
F1.7 23.6	F1.8 20.6	C0.0 23.3	C0.5 26.3
F2.0 23.6	F1.8 20.6	F0.6 22.4	C0.1 25.4
F1.7 23.2	F2.1 20.2	C0.3 23.7	C0.7 26.7
F2.1 23.6	F1.8 20.6	C0.9 24.6	C1.3 27.6
C0.8 27.5	C0.8 24.5	C1.7 25.8	C2.2 28.8
F0.1 26.3	C0.0 23.3	C2.9 27.6	C3.4 30.6

Sta		BS	HI	FS						
			1282.88							
69+00	1278.28			4.60			F2.2 / 23.3	F2.0 / 20.3	C0.7 / 24.3	C1.2 / 27.3
68+00	1282.16			0.72			F2.5 / 22.7	F2.4 / 19.7	C0.6 / 24.2	C0.9 / 27.2
		8.98	1291.75	0.11	1282.77					
67+00	1285.84			5.91			C0.0 / 26.7	C0.3 / 23.7	C3.2 / 26.1	C3.6 / 31.1
66+00	1288.04			3.71			F2.7 / 22.4	F2.6 / 19.4	C0.1 / 23.4	C0.4 / 26.4
65+00	1288.75			3.00			F1.7 / 23.6	F1.8 / 20.6	F2.7 / 19.3	F2.6 / 22.3
64+00	1289.25			2.50			F0.3 / 25.0	F0.9 / 22.0	F1.5 / 21.1	F1.2 / 24.1
BM #7				0.30	1291.45	1291.53				
63+00	1289.51									
62+00	1288.10									
61+00	1285.00									

Sta.		9/11/28 B.S	H.I	F.S							
BM #7			129466		129153						
63+00	128951			5.15			C0.6 27.8	C1.0 24.8		F0.9 22.0	F0.3 25.0
62+00	1288.16			6.56			C3.4 31.2	C3.3 28.8		C0.5 28.8	C0.2 26.8
61+00	1285.00			9.66			C1.1 27.5	C0.8 27.5		F0.6 22.4	F0.4 25.4
		2.36	128414	1288	1281.78	T.P.					
60+00	1281.67			2.47			F2.1 23.0	F2.2 20.0		F1.9 20.4	F1.7 23.4
59+00	1278.53			5.61			F2.2 22.9	F2.3 19.9		F2.1 20.3	F1.8 23.3
58+00	1276.68			7.46			F2.9 22.1	F2.6 19.1		F2.2 20.0	F2.4 23.0
		6.26	128326	7.14	1277.00	T.P.					
57+00	1276.33			6.93			F2.5 22.7	F2.7 19.1		F2.1 20.1	F1.9 23.1
56+00	127728			5.98			F0.5 25.6	F0.5 22.6		F1.0 21.8	F0.9 24.8
55+00	1277.52			5.74			C1.7 28.9	C1.7 25.9		C2.2 26.6	C2.3 29.6

Tobin & Spath Clear Snyder

23 3 1 5

Stg		3.5	41	1.3	
B.M. # 6			1283.26	4.62	1278.64
54+00	1275.97			7.29	
53+00	1272.62			10.64	
		1.69	1273.18	11.77	1271.49
52+00	1268.67			5.51	
51+00	1266.85			6.33	
		9.87	1280.58	2.47	1270.71
50+00	1267.45			5.73	
49+00	1270.47			10.11	
48+00	1275.62			4.96	
B.M. # 5.		1.74	1289.55	.372	1276.86
47+00	1281.08			8.47	
		11.68	1299.56	1.67	1287.88
46+00	1286.54			13.02	

B.M. # 6
1278.61

C 2.0 / 28.7	C 1.6 / 25.8		F 0.8 / 22.1	F 0.6 / 25.1
C 1.2 / 27.2	C 0.6 / 24.2		C 1.4 / 25.4	C 1.7 / 28.4
T.P. C 1.4 / 27.2	C 0.6 / 24.2		C 2.6 / 27.2	C 4.1 / 30.2
F 5.6 / 28.9	F 5.8 / 25.9		F 5.4 / 25.1	F 6.4 / 28.1
T.P. F 3.0 / 22.7	F 2.4 / 19.7		F 3.2 / 20.7	F 3.3 / 23.7
F 2.5 / 22.9	F 2.3 / 19.9		F 1.4 / 21.1	F 1.4 / 24.1
F 1.5 / 23.3	F 2.0 / 20.3		F 0.3 / 22.8	F 0.2 / 25.8
B.M. # 5 Elev. 05 1276.81 C 0.8 / 27.2	C 0.6 / 24.2		F 0.9 / 22.0	F 0.7 / 25.0
T.P. C 3.0 / 30.6	C 2.9 / 27.6		C 4.1 / 29.4	C 4.3 / 32.4

Sta	9/12/28	B.S.	HI	I.S.	
			1299.56		
45+00	1291.01			8.55	
44+00	1293.50			6.06	
		4.48	1300.59	3.45	1296.11
43+00	1295.00			5.59	
42+00	1296.50			4.09	
41+00	1298.00			2.59	
		9.84	1307.01	3.42	1297.17
40+00	1299.50			1.09	
BM #4		680	1307.03	680	1300.21
39+00	1301.00			6.03	
38+00	1302.09			4.94	
		2.66	1305.53	4.16	1302.87
37+50	1302.37			3.16	

[illegible] spokn Creek Snyder.

	C7.5 / 36.5	C6.8 / 33.5		C4.5 / 30.0	C4.4 / 33.0
	C4.0 / 32.7	C4.3 / 29.7		C2.3 / 26.7	C2.3 / 29.7
T.P	C0.8 / 27.3	C0.7 / 24.3		C1.9 / 26.1	C2.0 / 29.1
	F2.8 / 22.7	F2.9 / 19.7		F3.6 / 21.1	F3.4 / 24.1
	F3.4 / 24.9	F4.0 / 21.9		F3.8 / 21.5	F3.6 / 24.5
	C0.3 / 27.0	C0.5 / 24.0		F4.2 / 22.3	F4.6 / 25.3
B.M #4 1300.23	C1.6 / 22.8	C1.0 / 24.8		F2.5 / 19.6	F2.6 / 22.6
	C3.0 / 30.2	C2.6 / 27.2		F0.5 / 22.6	F0.5 / 25.6
T.P	C3.6 / 32.1	C3.9 / 29.1		C0.5 / 24.0	C0.6 / 27.0

Sta		B.S.	H.I.	F.S.		
			1305.53			
36+00	1301.83			3.70		
35+00	1300.48			5.05		
34+00	1298.72			6.81		
33+00	1296.96			8.57		
		1.10	1297.20	9.43	1296.10	T.P.
32+00	1295.30			2.00		
31+00	1293.44			3.76		
BM 3				2.98	1294.22	BM #3 1294.21
30+00	1291.68			5.52		
29+00	1289.92			7.28		
		2.12	1290.25	9.07	1288.13	T.P.
28+00	1288.24			2.01		

C0.1 / 26.9	F0.4 / 23.9	F1.4 / 21.4	F1.4 / 24.4	
F0.7 / 24.8	F1.0 / 21.8	F1.4 / 21.4	F1.5 / 24.4	
F1.3 / 23.8	F1.7 / 20.8	F1.8 / 20.6	F1.6 / 23.6	
F1.6 / 23.3	F2.0 / 20.3	F1.6 / 20.7	F1.2 / 23.9	
F2.2 / 22.9	F2.3 / 19.9	C0.1 / 23.4	C0.3 / 26.4	
F1.4 / 24.4	F1.3 / 21.4	C1.9 / 26.1	/ 29.1	
F1.3 / 24.4	F1.3 / 21.4	C1.0 / 24.8	C1.2 / 27.8	
F0.9 / 25.1	F0.8 / 22.8	C3.9 / 29.1	C4.0 / 32.1	
F2.8 / 22.6	F2.5 / 19.6	F3.0 / 19.9	F2.9 / 22.9	

Sta		B.S	H.I	F.S		
			1290.25			
27+00	1287.12			3.13		
26+00	1286.64			3.61		
25+00	1286.82			3.43		
24+00	1287.63			2.62		
BM #2		7.39	1294.54	3.10	1287.15	
23+00	1289.07			5.47		
22+00	1291.19			3.35		
				0.04	1294.50	T.P. on Rock 25' Rt.
21+00	1293.93					
20+00	1297.24					

F2.1 / 22.9	F2.3 / 19.9		F2.9 / 19.7	F3.0 / 22.7
F1.5 / 23.9	F1.6 / 20.9		C1.3 / 25.2	C1.8 / 28.2
F1.4 / 24.1	F1.5 / 21.0		C0.5 / 24.0	C1.2 / 27.0
F0.2 / 25.3	F0.7 / 22.3	BM #2. 1287.15	F0.8 / 22.1	F0.5 / 25.1
F2.3 / 22.6	F2.5 / 19.6		F2.3 / 19.9	F2.2 / 22.9
F0.4 / 25.4	F0.6 / 22.4		F1.9 / 20.5	F1.7 / 23.5
	28.0		22.5	
	27.0		22.0	

Sta	9/13/28	B.S.	H.I.	F.S.		[illegible]	[illegible]				
		9.33	1303.83		1294.50	T.P.					
21+00	1293.93			9.90			C3.0 / 30.8	C3.0 / 27.8		F1.0 / 21.8	F0.7 / 24.8
20+00	1297.24			6.59			C2.4 / 30.9	C2.4 / 26.9		F1.1 / 21.7	F0.9 / 24.7
19+00	1299.48			4.35			C2.9 / 30.2	C2.6 / 27.2		F0.9 / 22.0	F0.6 / 25.0
		6.68	1306.92	3.59	1300.24	T.P.					
18+00	1302.78			4.14			F0.2 / 25.9	F0.3 / 22.9		F1.9 / 20.5	F1.8 / 23.5
17+00	1303.98			2.94			F0.9 / 23.8	F1.7 / 20.8		F2.9 / 19.7	F3.0 / 22.7
16+00	1304.25			2.67			F2.2 / 22.9	F2.3 / 19.9		F1.6 / 20.9	F1.0 / 23.9
15+00	1304.37			2.55			F1.9 / 23.3	F2.0 / 20.3		C1.6 / 25.7	C2.0 / 28.7
		1.70	1305.68	2.94	1303.98	T.P.					
14+00	1303.63			2.05			F0.8 / 24.7	F1.1 / 21.7		C0.3 / 23.7	C0.5 / 26.7
B.M. #1				2.59	1303.09	B.M. #1 1303.10					
13+00	1300.95			4.73			C0.9 / 27.5	C0.8 / 24.5		C1.5 / 25.5	C1.6 / 28.5

Stg		B.S.	H.I.	F.S.						
			130568							
12+00	1297.40			8.28			C1.1 / 27.5	C0.8 / 24.5	C1.9 / 26.1	C2.4 / 29.1
		2.24	129573	12.19	129349	T.P.	F3.5 / 24.3	F3.7 / 21.3	F3.7 / 21.8	F3.2 / 24.3
11+00	129385			1.88						
							F3.2 / 23.9	F3.5 / 20.9	F3.7 / 21.3	F3.5 / 24.5
10+00	1290.30			5.43						
		2.50	1289.60	8.63	1287.10	T.P				
9+00	1286.75			2.95			F1.5 / 25.0	F0.9 / 22.0	F1.7 / 20.8	F1.6 / 23.8
							C1.9 / 28.4	C1.4 / 25.4	C0.2 / 23.6	C0.5 / 26.6
8+00	1283.20			6.40						
							C2.9 / 30.9	C3.1 / 27.9	C1.3 / 25.2	C1.4 / 28.2
7+00	1279.65			9.95						
		5.08	1283.67	11.01	1278.59	T.P				
6+00	1276.10			7.57			C4.1 / 31.7	C3.6 / 28.7	C0.3 / 23.7	C0.5 / 26.7
							C3.6 / 29.7	C2.3 / 26.7	C0.0 / 23.3	F0.1 / 26.3
5+00	1272.55			11.12						
		1.60	1273.78	11.49	1272.18	T.P				
4+00	1269.59			4.19			C1.4 / 28.2	C1.3 / 25.2	F0.3 / 22.9	F0.2 / 25.9

Sta		B.S.	H.I	F.S	
			127378		
3+00	126780			5.98	
2+00	1266.60			7.18	
1+00	126540			8.38	
0+00	126420				
B.M #0				8.47	12653.1

C-0.7 / 27.0	C0.5 / 29.0		F1.2 / 21.5	F1.3 / 24.5
F0.4 / 25.3	F0.7 / 22.3		F1.2 / 21.5	F1.8 / 24.5
F1.2 / 24.4	F1.3 / 21.4		F1.5 / 21.1	F1.5 / 24.1

chk. 04
1265.35
N.W. Cor
N. Headwall left. End of Project

Finished Grade 10/17/28 BM #10

Sta		B.S.	H.I	F.S.	1251.69
104+00	1253.36			4.15	✓
+50	1253.34			4.17	✓
105+00	1253.17			4.34	✓
+50	1252.86			4.65	✓
106+00	1252.48			5.03	F.05 ✓
+50	1252.10		1257.51	5.41	F.05 ✓
107+00	1251.72			2.57	F.05 ✓
+50	1251.34			2.95	F.0.5 ✓
108+00	1250.95			3.34	✓
+50	1250.52			3.77	C0.5
109+00	1250.16			4.13	✓
+50	1249.77			4.52	✓
110+00	1249.38			4.91	✓
+50	1248.99			5.30	✓
111+00	1248.59			5.70	✓
+50	1248.19			6.10	✓
112+00	1247.79			6.50	✓
+50	1247.33	6.25	1254.29	7.04 B.M.	#11 1248.04

Peg these notes up the sheet

Whiskie Rain
Stoken
Snyder

Chk. .04

586 1251.65

1251.22

1248.04
6.25
1254.29
3.07
1251.22
6.29
1257.51
5.86
1251.65

1254.29
0.95
3.34

10/17/38 Elev BM #1

Sta		B.S.	H.I.	F.S.	1248.04
		1.13	1249.17		
113+00	1246.77			2.40	✓
+50	1246.10			3.07	✓
114+00	1245.31			3.86	✓
+50	1244.47			4.70	✓
115+00	1243.62			5.55	✓
+50	1242.78			6.39	✓
116+00	1241.93			7.24	✓
+50	1241.09			8.08	✓
117+00	1240.24			8.93	✓
+50.	1239.40			9.77	123940 ✓
118+00	1238.55	0.84	1240.24	1.69	✓
+50	1237.71			2.53	✓
119+00	1236.86			3.38	✓
+50	1236.02			4.22	✓
120+00	1235.17			5.07	✓
+50	1234.50			5.74	✓
121+00	1234.13			6.11	✓
+50	1234.08		C 0.5	6.16	

T.P.

1248.04
1.13
1249.17
9.77
1239.40
0.84
1240.24

Sta		B.S.	H.I	F.S.	
			1240.24		
122+00	1234.34			5.90	✓
+50	1234.76			5.48	✓
123+00	1235.18	6.43	1241.19	6.01	✓
+50	1235.60			5.59	✓
124+00	1236.02			5.17	✓
+50	1236.44			4.75	✓
125+00	1236.86			4.33	✓
+50	1237.28			3.91	✓

1241.19
6.70
1234.49

1240.24
5.48
1234.76
6.43
1241.19

New BM N.E. Cor of East H.W
Sta 121+85 Elev. 1234.49

Finished Grade BM #8

Sta		B.S.	H.I	F.S.	Elev 1265.12
		251	126763		
81+50	1263.04			4.59	
82+00	1262.76			4.87	
+50	1262.00			5.63	
83+00	1261.00			6.63	1261.00
+50	1260.00	1.12	126212	2.12	
84+00	1259.00			3.12	
+50	1258.00			4.12	
85+00	1257.00			5.12	
+50	1256.00			6.12	
86+00	1255.00			7.12	
+50	1254.00			8.12	
87+00	1253.08			9.04	1253.02
+50	1252.34	388	1256.90	4.56	
88+00	1251.77			5.13	
+50	1251.37			5.53	
89+00	1251.06			5.84	
+50	1250.74			6.16	
90+00	1250.43			6.47	1250.43

Whisler Notes
Rand Level
Spohn Rod
Snyder ---- Chain

10/20/28. Cloudy Cold 56

T.P.

1265.12
2.51
1267.63
6.63
1261.00
1.12
1262.12
9.04
1253.08
4.24
1257.32
6.89
1250.43

67.40
1263.04
436
1267.40
642
1260.98
2.02
1263.00
998
1253.02
388
1256.90
647
1250.43
306
1253.49

555
689
29
126300
6000
.300

T.P

Sta		BS.	H.I.	FS	Elev.
		3.06	1253.49		
+50	1250.12			3.37	
91+00	1249.94			3.55	
+50	1250.01			3.48	
92+00	1250.27			3.22	
+50	1250.78	1.36	1253.73	2.95	
93+00	1251.42			2.31	
+50	1252.06			1.67	
94+00	1252.70			1.03	1252.70
+50	1253.24	4.49	1257.19	3.95	
95+00	1253.56			3.63	
+50	1253.64			3.55	
96+00	1253.50			3.69	
+50	1253.25			3.94	
97+00	1253.00			4.19	
+50	1252.75			4.44	
98+00	1252.50			4.69	
+50	1252.25			4.94	1252.25
99+00	1252.00	3.59	1255.84	3.84	

1250.43
3.46
1253.89
1.36
1252.53

1237.49
0.79
2.71
4.84
1252.37
1.36
1253.73
1.03
1252.70
4.49
1257.19
4.94
1252.25
3.59
1255.84

367
295
78

B.M.9 1252.37
Chk.02 1252.35
1253.49
1.14
1252.35

T.P

Sta		BS	HI	F.S.	Elev
			1255.84		
+50	1251.75			4.09	✓
100+00	1251.57			4.27	✓
+50	1251.51			4.33	✓
101+00	1251.58			4.26	✓
+50	1251.76			4.08	✓
102+06	1252.07			3.77	✓
+50	1252.50			3.34	

1255.84
414
1251.70

BM #10
1251.69

BM	5.62	1270.97		1265.35
1			5.57	1265.40
2			4.37	1266.60
3			3.17	1267.80
4			1.38	1269.59
	11.58	1280.77	1.78	1269.19
5			8.22	1272.55
6			4.67	1276.10
	10.42	1289.55	1.64	1279.13
7			9.90	1279.65
8			6.35	1283.20
9			2.80	1286.75
	8.81	1297.13	1.23	1288.32

F 1.3 / 24.4

F 1.6 / 24.1

F 0.7 / 25.3

F 1.9 / 24.5

C 0.5 / 27.0

F 1.5 / 24.5

C 1.3 / 28.2

F 0.9 / 25.9

C 3.4 / 29.7

F 0.2 / 26.3

C 3.9 / 31.7

F 0.1 / 26.7

C 2.9 / 30.9

C 1.0 / 28.7

C 1.6 / 28.4

C 0.3 / 26.6

F 0.9 / 25.0

F 1.9 / 23.8

		1297.13		
10			6.83	1290.30
11			3.28	1293.85
	9.97	1306.11	0.49	1296.64
12			8.71	1297.40
13			5.16	1300.95
BM#1	4.21	1307.31	2.67	1304.44 / 1304.10
14			3.68	1303.63
15			3.24	1304.07
16			3.56	1303.75
	3.42	1305.56	5.17	1302.14
17			2.08	1303.48
18			2.88	1302.68
19			6.08	1299.48

F3.5 / 23.9

F3.5 / 24.3

F3.9 / 24.3

F3.5 / 24.3

C0.9 / 27.5

C2.2 / 29.1

C0.6 / 27.5

C1.3 / 28.5

F0.8 / 24.7

C0.5 / 26.7

F1.7 / 23.3

C2.3 / 28.7

F1.6 / 22.9

F0.5 / 23.9

F0.6 / 23.8

F2.3 / 22.7

C0.0 / 25.7

F1.7 / 23.5

C2.5 / 30.2

F0.6 / 25.0

	2.37	1300.73	7.20	1298.36	
20			3.49	1297.24	
21			6.80	1293.93	
22			9.54	1291.19	
	0.88	1291.68	9.93	1290.80	
23			2.61	1289.07	
BM#2	4.46	1291.61	4.46	1287.22	1287.15
24			3.98	1287.63	
25			4.79	1286.82	
26			4.97	1286.64	
	10.40	1295.54	6.47	1285.14	
27			8.42	1287.12	
28			7.30	1288.24	
29			5.62	1289.92	

C 2.5 / 30.9

F 0.9 / 24.7

C 3.2 / 30.8

F 0.7 / 24.8

F 0.4 / 25.4

F 1.6 / 23.5

F 2.3 / 22.6

F 2.0 / 22.9

F 0.3 / 25.5

F 0.6 / 25.1

F 1.5 / 24.1

C 1.3 / 27.0

F 1.5 / 23.9

C 2.0 / 28.2

F 1.9 / 22.9

F 2.7 / 22.7

F 2.7 / 22.6

F 2.8 / 22.9

F 0.8 / 25.1

C 4.0 / 32.1

				BM	109480
STA		B.S.	H.I.	FS	
STA		284	1097.64	6.60	1091.04
		209	1093.13	6.92	1086.21
101+00	1083.38	1.70	1087.91	4.53	
+50	1082.79			5.12	
102+00	1082.10			5.70	
+50	1081.66			6.25	
103+00	1081.24			6.67	
+50	1080.94			6.97	1080.94
104+00	1080.76	368	1084.62	3.86	
+50	1080.64			3.98	
105+00	1080.52		F0.5	4.10	
+50	1080.46			4.22	
106+00	1080.28		F0.5	4.34	
+50	1080.16		F0.5	4.46	
107+00	1080.04		F0.5	4.58	
+50	1079.92		F1.0	4.70	
108+00	1079.80		F1.0 F0.5	4.82	1078.80
+50	1079.68	504	1083.84	4.16	
109+00	1079.56		F0.5	4.28	

		109480
		284
TP		1097.64
		6.60
TP		1091.04
		209
		1093.13
		6.92
		1086.21
		1.70
		1087.91
		6.97
		1080.94
TP		3.68
		1084.62
		5.82
		1078.80
		504
		1083.84

		BS	H.I	FS		
Sta			1083.84			
+50	1079.44		F0.5	4.40		
110+00	1079.32			4.52		
+50	1079.20			4.64		
111+00	1079.08			4.76		
+50	1078.96			4.88		
112+00	1078.84		C0.5	5.00		
+50	1078.72		C0.5	5.12		
113+00	1078.60			5.24	1078.60	T.P
+50	1078.48	4.20	1082.80	4.32		
114+00	1078.36			4.44		
114+50	1078.09			4.71		
114+98	1078.76		F0.6	4.04		
115+50	1079.45		F2.0	3.35		B.M. #10
		4.93		4.93	1077.87	

1083.84
5.24
1078.60
4.20
1082.80
4.93
1077.87

		1295.54					
30			3.86	1291.68		F 1.2 / 24.4	C 1.2 / 27.8
BM#3	5.54	1299.75	1.22	1294.32	1294.21		
31			6.31	1293.44		F 1.9 / 24.4	C 2.6 / 29.1
32			4.55	1295.20		F 2.3 / 22.9	C 0.2 / 26.4
33			2.79	1296.96		F 1.7 / 23.3	F 1.3 / 23.9
34			1.03	1298.72		F 1.3 / 23.8	F 1.6 / 23.6
slope stake at L 84+00			2.33	1297.42			
35				1300.18		24.8	24.4
36				1301.83		26.9	24.4
37							
38							
39							

5/20/29

Stake			Fishing Rod Rise	
34+00	9.65	1307.07		1297.42
35			6.59	1300.48
36			5.24	1301.83
37			4.70	1302.37
38			4.98	1302.09
39			6.07	1301.00
BM #4	2.44	1300.93	8.58	1298.49
				1300.23
40			1.43	1299.50
41			2.93	1298.00
42			4.43	1296.50
43			5.93	1295.00
	3.51	1300.42	4.02	1296.91
44			6.92	1293.50

F 0.3 / 24.8

F 1.1 / 24.4

C 0.0 / 26.9

F 1.6 / 24.7

C 4.1 / 32.1

C 0.2 / 27.0

C 2.9 / 30.2

F 0.6 / 25.6

C 1.5 / 27.8

F 2.5 / 22.6

F 1.7 / 27.0

F 1.7 / 25.3

F 3.5 / 24.9

F 3.3 / 24.5

F 2.9 / 22.7

F 3.2 / 24.1

C 0.9 / 27.3

C 1.9 / 29.1

C 4.0 / 32.7

C 2.2 / 29.7

	1300#2				
45		9.41	1291.01	C 7.5 / 26.5	C 7.6 / 33.0
46		13.88	1286.54	C 3.1 / 30.8	C 3.1 / 32.7
NW ∠ of W Headwall		12.44	1287.98		
47			1281.08	27.2	25.0
BM#5			1276.81		
48			1275.62	23.3	25.8
49			1270.47	22.9	24.1
50			1267.95	22.7	23.7
51			1266.85	28.9	28.1
52			1268.67	27.2	30.2
53			1272.62	21.2	28.4
54			1275.97	28.7	25.1
BM#6			1278.61		

		5/29/29		M Richey F Richey	C [illegible] T Kiser		233			
BM 133+02	3.37	1237.57			1234.20					
132			3.07	1234.50		F1.9 / 23.2	F2.1 / 20.2		F1.1 / 21.7	F0.9 / 24.7
131			1.50	1236.27		F2.2 / 22.5	F2.5 / 19.5		F1.3 / 21.3	F1.0 / 24.3
	9.51	1244.60	2.48	1235.09						
130			6.10	1238.50		F1.0 / 24.3	F1.3 / 21.3		C0.5 / 24.1	C0.8 / 27.1
129			3.71	1240.59		C0.7 / 27.4	C0.7 / 24.4		C1.6 / 25.7	C1.9 / 28.7
128			3.34	1241.26		F0.3 / 25.5	F0.5 / 22.5		F1.3 / 21.3	F1.0 / 24.3
127			4.98	1239.62		F0.2 / 25.2	F0.7 / 22.2		F0.7 / 22.2	F0.5 / 25.2
	2.50	1241.92	5.18	1239.42						
126			3.95	1237.97		F0.3 / 25.6	22.6	special	21.8	F0.2 / 24.8
125			5.06	1236.86		F1.6 / 24.4	21.4	special	23.1	C0.8 / 27.1
124			5.90	1236.02		C0.6 / 26.2	—		—	C1.1 / 27.5
	3.51	1239.04	6.39	1235.53						

		1239.04			
123			3.86	1235.18	
NW/4 W Headwall 4					
122			4.70	1234.34	
NW/4 W Headwall	4.88	1239.31	4.88	1234.16	1234.43
121			5.18	1234.13	
120			4.14	1235.17	
	7.78	1243.59	3.50	1235.81	
119			6.73	1236.86	
118			5.04	1238.55	
117			3.35	1240.24	
116			1.66	1241.93	
	8.50	1251.04	1.05	1242.54	
115			6.42	1243.62	

F1.8 / 23.8	—	C0.1 / 25.9	—
F1.7 / 23.9	—	F1.3 / 24.4	—
F0.7 / 24.8	—	F1.0 / 24.7	—
F0.5 / 25.1	—	F0.5 / 25.4	—
C0.0 / 25.9	—	C3.0 / 29.9	—
F0.7 / 24.5	—	C1.3 / 27.6	—
F0.5 / 24.8	—	C0.7 / 27.2	—
F1.3 / 23.9	—	C0.4 / 26.6	—
F1.8 / 25.3	—	F0.3 / 26.6	—

		1251.04			
114			5.73	124.31	
BM#11	2.92	1250.96	2.92	1248.12	1248.04
113			4.19	124.77	
112			3.17	124.79	
111			2.37	124.59	
	5.50	1254.38	2.08	1248.88	
110			5.00	249.38	
109			4.22	250.16	
108			3.43	250.35	
107			2.66	251.72	
106			1.90	252.48	

C 0.1 / 25.6

C 0.5 / 27.2

C 0.5 / 26.6

C 1.3 / 28.1

E 0.5 / 25.3

C 0.5 / 26.9

F 0.2 / 25.6

C 0.8 / 27.3

F 1.1 / 24.2

C 0.4 / 26.9

F 2.1 / 23.3

F 0.8 / 24.6

F 2.7 / 22.4

F 1.8 / 23.5

F 2.1 / 22.7

F 0.6 / 24.7

F 1.4 / 23.5

F 0.7 / 24.8

		1254.38			
105			1.21	1253.17	
	5.48	1257.15	2.71	1251.67	
104			3.79	1253.36	
103			4.22	1252.93	
102			5.08	1252.07	
BM#10			5.97	1251.68	1251.69
101				1251.58	
100					
99					
98					
97					
96					

F1.5 / 22.6

F0.6 / 24.8

F0.5 / 25.1

C0.5 / 26.6

C0.0 / 25.6

C1.5 / 25.2

F1.6 / 23.5

F0.7 / 24.5

22.7

22.7

		5/29/31 Richey Rand	Girard Kiser.	
BM#10	4.10	1255.79		1251.69
101			4.21	1251.58
100			4.22	1251.57
99			3.79	1252.00
98			3.29	1252.50
97			2.79	1253.00
	5.63	1257.32	4.10	1251.69
96			3.82	1253.50
95			3.76	1253.56
94			4.62	1252.70
93			5.90	1251.42
BM#9	1.66	1254.03	4.93	1252.39 1252.37

F2.1 27.7

F2.4 27.7

F0.8 25.6

C1.1 27.3

C0.8 27.0

C1.0 27.5

F0.2 25.4

C0.0 25.9

F1.3 24.1

F0.2 25.3

F1.3 23.5

C0.1 25.6

C0.0 26.3

C0.6 26.3

F0.6 25.4

F0.2 25.4

F0.2 25.4

C0.2 26.2

NE Cor E Hall

Sta. 121+85 BS H.I. ℄

B.M.

1234.49 8.31 1242.80 1238.0

126+00 25/5.3 14/5.5 12/5.0 ℄/4.8 13/5.0 15/5.6 23/5.3

1235.6

127+00 25/3.7 13/4.2 ℄/4.2 7/4.5 23/3.6

1.60 1241.20

3.71 1244.91 1240.1

128+00 25/4.0 6/4.5 ℄/4.8 6/4.6 9/4.2 10/4.8 25/4.8

1241.9

128+46 25/2.2 9/2.5 3/3.0 ℄/3.0 8/2.6 25/2.0

1240.3

129+00 25/3.2 11/3.9 5/4.5 ℄/4.6 7/4.2 9/3.5 25/2.3

1237.2

129+80 ℄/2.7 7/3.3 5/3.6 12/4.3 25/6.6

1236.8

130+00 25/7.1 18/7.3 14/7.4 13/8.2 ℄/8.1 5/7.8 6/8.4 11/6.1 25/5.9

11/24/28 Cloudy

Extension Baldwins Mills

℄

70 45' Spk in CEI #575493

PC T Sta 129+00

113 77' Spk in ℄ CEI # 575494

TP

770.14 Aug 58

Spk in CEI # 575495

86 58

PI Sta 125+35 00

Tacked Hub

35

170° 15'

96 27

170-06 m Aug 58

Spk in CEI # 575496

H.I 1244.91

1234.3

131+00	25 / 11.5	15 / 10.9	14 / 11.3	12 / 10.5	℄ / 10.6	6 / 10.5	8 / 11.5	9 / 10.7	25 / 10.0

1233.2

132+00	25 / 12.6	15 / 12.0	14 / 12.4	12 / 11.8	℄ / 11.7	4 / 12.0	5-7 / 12.6	8 / 12.0	25 / 11.3

1020 123471

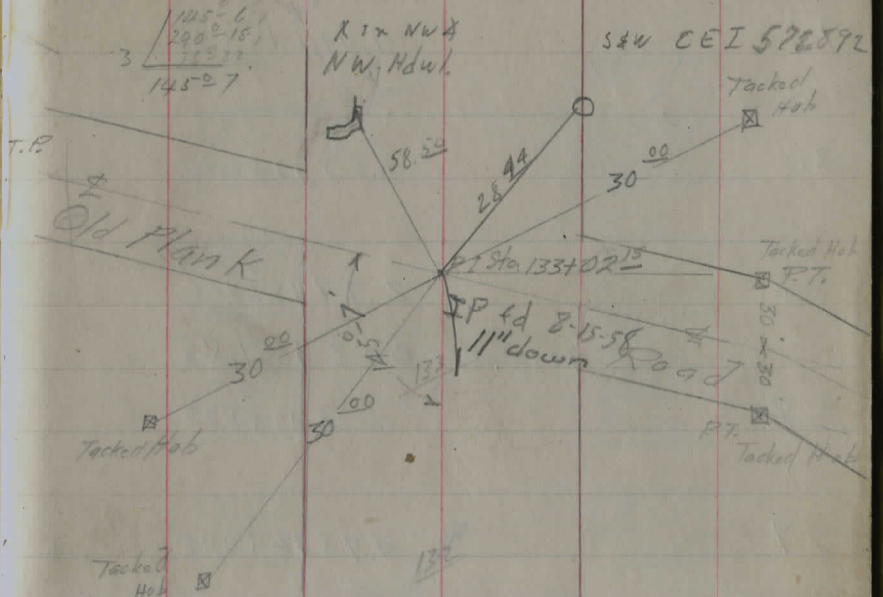
223 1236.94

133+00	24 / 5.1	22-23 / 6.9	18 / 4.1	℄ 1232.8 / 4.1		21 / 4.6	24-25 / 5.6		26 / 4.1

E-W Cross Road	100 / 5.3	50 / 4.8	℄ / 4.1	50 / 3.5	100 / 2.8	

BM
274 1234.30

BM Spike in root 18" Maple Located 150' N20°W of Intersection of Baldwins Cor N. and Old Rank Road Elev – 123420



		1254.03		
92			3.76	1250.27
91			4.09	1249.94
90			3.63	1250.43
89			2.97	1251.06
	6.48	1258.03	2.48	1251.55
88			6.26	1251.77
87			4.95	1253.08
86			3.03	1255.00
	8.77	1265.55	1.25	1256.78
85			8.55	1257.00
84			6.55	1259.00
83			4.55	1261.00

F1.7 23.8	F1.5 23.8
F1.7 23.8	F0.6 25.2
F1.1 24.2	F0.3 25.7
F0.2 25.6	C0.5 26.4
F0.7 25.0	C0.7 26.7
F2.0 22.7	F0.8 25.0
C0.7 26.7	F1.4 24.2
C1.3 28.2	C1.5 27.9
F0.8 24.7	F0.7 25.1
F2.5 22.6	F1.8 23.5

		1265.55			
82			2.79	1262.76	
	2.49	1267.54	0.50	1265.05	
81			4.70	1262.84	
BM#8	2.49	1267.61	2.49	1265.05	1265.12
80			6.37	1261.24	
79			8.21	1259.40	
	3.26	1261.45	9.42	1258.19	
78			3.47	1257.98	
77			4.08	1257.37	
76			3.87	1257.58	
75			2.73	1258.72	
74			0.91	1260.54	
T.P. Hub on W at 74+00	12.21	1270.77	2.89	1258.56	
73			7.59	1263.18	

C0.4 / 26.6

C0.3 / 26.6

C2.2 / 29.0

C3.9 / 31.4

C1.5 / 28.4

C2.4 / 29.7

F1.5 / 23.3

F1.2 / 23.0

F3.6 / 24.1

F3.6 / 24.3

F2.5 / 22.5

F1.0 / 23.5

F1.0 / 25.1

C1.9 / 27.8

F1.5 / 23.6

C0.5 / 26.3

F2.0 / 23.6

C0.2 / 25.4

F2.3 / 23.2

C0.7 / 26.7

		1270.77		
72			4.13	1266.64
	11.26	1280.68	1.35	1269.42
71			10.16	1270.52
70			6.28	1274.40
69			2.40	1278.28
	10.50	1290.82	0.36	1280.32
68			8.66	1282.16
67			4.98	1285.84
66			2.78	1288.04
65			2.07	1288.75
64			1.57	1289.25
	7.92	1295.08	3.66	1287.16
63			5.57	1289.51
BM#7	3.56	1295.09	3.56	1291.53

F 2.0
23.6

C 1.3
27.6

C 0.5
27.5

C 1.9
28.8

F 0.2
26.3

C 3.2
30.6

F 2.0
22.3

C 1.1
27.3

F 2.3
22.4

C 0.8
27.2

F 0.2
26.7

C 3.5
31.1

F 2.5
22.4

C 0.2
26.4

F 1.6
23.6

F 2.5
22.3

F 0.3
25.0

F 2.1
24.1

C 0.9
27.8

F 0.7
25.0

1295.09

62 — 6.99 / 1288.10

61 — 10.09 / 1285.00

1.84 / 1286.65 — 10.28 / 1284.81

60 Hubon W side 60+00 — 4.98 / 1281.67

7.07 / 1279.58

17

537

8665
8.77
1277.88

83.11
72.88
5.23

8645
5.37
81.28

Not set
℄ of x road

31.2 — 26.8

C 1.0 / 27.5

F 0.2 / 20.4

F 2.1 / 23.0

F 1.7 / 23.4

83.1
1279.58

7.53
4
3.93

BM#5	7.83	1284.64		1276.81
47			3.56	1281.08
48			9.02	1275.62
	0.72	1272.93	12.93	1271.71
49			1.96	1270.47
50			4.98	1267.45
51			5.58	1266.85
52			3.76	1268.67
	10.66	1280.74	2.25	1270.08
53			8.12	1272.62
54			4.77	1275.97
BM#6	21.2	1280.73	2.12	1278.62 / 1278.61
55			3.21	1277.52
56			3.45	1277.28

C 0.7 / 27.2

F 0.8 / 25.0

F 1.6 / 23.5

C 0.3 / 25.8

F 2.4 / 22.9

F 1.3 / 24.1

F 2.6 / 22.7

F 3.1 / 22.7

F 5.7 / 28.9

F 5.1 / 28.1

C 0.5 / 27.2

C 3.3 / 30.2

C 1.1 / 27.2

C 1.8 / 28.4

C 1.5 / 28.3

F 0.8 / 25.1

C 1.6 / 28.9

C 2.0 / 29.6

F 0.5 / 25.6

F 0.7 / 24.8

Check BM on North and South Center Road

BM No 7 X on Wing Wall
Elev 1193.66
Bostwick Corners

Elev Conc. Pvt. 1264.14

133+00.88

Table IX.—Calculation of Earthwork.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if w =16.2 and h =5.3, cu. yds. =1.48+.028+.089 =1.597 cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) =h, and ½ the roadbed =w, add the triangles formed by taking the distance out to each break in turn (=w's) by the difference between the cuts (or fills) on each side of it (=h's) always subtracting the outer from the inner.

Distances from Center of Roadway for Cross-Sectioning.

Roadway 16 feet wide. Side Slopes 1 on 1½.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29 2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

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